

WATER USE LICENCE APPLICATION Geohydrological Assessment

4 October 2022

Prepared for:

Wisteria Boerdery (Pty) Ltd PO Box 254 Patensie 6335

Contact: Mr R Du Preez Cell: 083 330 7239

Email: deleen@wisteriafarm.co.za

by

DHS GROUNDWATER CONSULTING SERVICES

PROJECT TEAM

K Jeppesen

DH Stroebel

Report: DHS-22-192

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Authors:

Keegan Jeppesen (MSc. Hydrogeology) Hydrogeologist

Divan Stroebel (Pr.Sci.Nat, GWD, MGSSA, BSc Hons. Geology) Hydrogeologist - Director DHS Groundwater Consulting Services



9 Schubert Road Walmer Heights Port-Elizabeth 6070 South Africa

T+27 (0) 82 099 2366 E divan@dhsgroundwater.co.za W https://dhsgroundwater.co.za

Main Authors Resume

Divan Stroebel is a SACNASP registered and active member of the Groundwater Division, the Geological Society of South Africa, hydrogeologist and professional geoscientist with more than 16 years of industry experience. He obtained his B.Sc. (Geology) degree in 2005 and his B.Sc. Honours (Geology) degree in 2006 from Stellenbosch University. From 2007, he worked throughout Africa as an exploration geologist in base metal, iron ore and gold exploration. In 2009 he joined a hydrogeological consultancy and completed additional groundwater modules at the Institute for Groundwater Studies (IGS), University of Free State. He was employed by mining giant, Rio Tinto in 2010 in Guinea as a Geologist, after which he was the Superintendent Geologist at Goldfields' Kloof mine from 2012. He joined AEON at the Nelson Mandela University (NMU) in 2014 as Associate Research Manager for the Karoo Shale Gas Research Programme- focused on Karoo hydrogeology.

Divan's technical experience includes all aspects of mineral exploration, extraction and reserve management as well as hydrogeological assessments, aquifer characterisation, groundwater supply development, groundwater and surface water characterisation and monitoring as well as water quality assessments.

Divan is very active in the hydrogeological community and has attended, presented at and coorganised numerous water-research workshops and conferences. In June 2016, he was appointed as a visiting researcher at Queen's University, Belfast. In China (2017), he successfully completed an international training programme on the Sustainable Development of Water Resources in Arid Regions for Developing Countries.

During his time at AEON, Divan researched the Groundwater Hydrochemistry and Aquifer Connectivity Baseline of the Eastern Cape Karoo. In anticipation of the controversial hydraulic fracturing planned for the Eastern Cape, he has obtained unique experience in the determination of salinity, aquifer yields and groundwater levels of the Karoo's scarce groundwater resources and has published an article in a special publication by the Geological Society of London on fractured aquifers on the topic. https://sp.lyellcollection.org/content/479/1/129

Divan is the founder and owner of DHS Groundwater Consulting Services and leads the team as principal hydrogeologist, overseeing all projects from inception to completion.

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I consider myself bound to the rules and ethics of the South African Council for Natural Scientific Professions (SACNASP);

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- All the particulars furnished by me in this document are true and correct.

Divan Stroebel (Pr.Sci.Nat, GWD, MGSSA, B.Sc Hons. Geology)

Hydrogeologist

Director: DHS Groundwater Consulting Services (Pty) Ltd

SACNASP Registration Number 400371/12



9 Schubert Road Walmer Heights Port-Elizabeth 6070 South Africa

T +27 (0) 82 099 2366 E divan@dhsgroundwater.co.za W https://dhsgroundwater.co.za

Executive Summary

Wisteria Boerdery (Pty) Ltd will be using groundwater for the irrigation of citrus orchards and other crops on the farms Buffels Hoek 180 (Portion 2) and Loerie River 436 (Portion 46), hereafter also referred to as the site. Groundwater will be abstracted from boreholes with volumes exceeding General Authorisation (GA) and therefore the water use needs to be licensed. Wisteria Boerdery (Pty) Ltd therefore appointed DHS Groundwater to conduct a geohydrological assessment as part of the Water Use License Application (WULA).

The most important findings of the assessment are summarised in the following table:

Geohydrological Characteristics	Farm Buffels Hoek 180 and Loerie River 436
Geology:	Enon and Kirkwood Formations of the Uitenhage Group. The Enon conglomerates are overlain by Kirkwood Formation mudstone and sandstone and both overlain by river gravel terraces. The regional scale Gamtoos fault (trending northwest-southeast) is located +- 8.5km to
	the north east of the site
Aquifer Types:	Hard rock/Secondary fractured aquifers.
Aquifer Classification:	Major Aquifer System
Borehole Yields:	0.91 – 10.49 L/s
Depth to Water Table:	4.10 – 31.44 meters below ground level
Groundwater Quality:	All the major ions and the majority of trace elements comply with (SANS 241-1:2015, edition 2) drinking water standards. The levels of Fe and Mn are notable elevated. TDS of 390 - 691 mg/l.
Regional Groundwater Use:	Agriculture (Irrigation & stock watering)
Mean Annual Rainfall:	587 mm/a
Recharge:	25 - 37 mm/a (4.3% - 6.3% of MAP)
Groundwater available for abstraction from GRU:	0.961 Mm³/a

Geohydrological Characteristics	Farm Buffels Hoek 180 and Loerie River 436		
Water Demand:	0.799 Mm³/a		
Cumulative Sustainable Yield from tested borehole(s):	0.887 Mm³/a		
Volume to be applied for:	0.799 Mm³/a		

Based on the field work, interpretation of available and newly acquired data, the abstraction of groundwater from the site will have an overall "negligible – negative" impact on the investigated geohydrological environment after implementation of appropriate mitigation measures. During the rating and ranking procedure of impacts, all identified impacts could be countered by appropriate mitigation.

Based on the water balance results, the applied allocation of 0.799 Mm³/annum places the application in a Category B abstraction (medium scale abstractions 60-100% recharge to the GRU). The tested boreholes will be able to supply in 100% of the demand, as well as the applied volume.

From a water quality point of view, elevated Iron and Manganese exceeding SANS241-1:2015 drinking water limits were reported in the boreholes located within the site as well as two other boreholes located outside the site sampled during the hydrocensus. Although the major elements are within the recommended drinking water limits, the elevated Iron and Manganese levels deem the groundwater unfit for human consumption.

It is the assessor's professional opinion that adequate information was available to appropriately assess the impact of groundwater abstraction from the production boreholes on the geohydrological environment. Based on the results, it is recommended that the application be approved. It is however imperative that the applicant implements the proposed "Environmental Management & Groundwater Monitoring Program". Production boreholes should be equipped as follow:

- Installation of a 32 mm LDPE observation pipe from the pump depth to the surface, open at the bottom. This allows for a 'window' of access down the borehole which enables manual water level monitoring and can house an electronic water level logger if required.
- Installation of a sampling tap (to monitor water quality).
- Installation of a flow volume meter (to monitor abstraction rates and volumes).
- The appropriate borehole pump must be installed, i.e., not an over-sized pump that is choked with a gate valve. If the monitoring shows that more water can be abstracted, then duty cycles (i.e., the duration of pumping time) may be increased, and not the flow rate.



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List of Abbreviations

Term	Definition
%	Percentage
CDT	Constant Discharge Test
CFU	Colony Forming Unit
DEA	Department of Environmental Affairs
DRO	Diesel Range Organics
DWAF	Department of Water Affairs & Forestry
DWS	Department of Water & Sanitation
EC	Electrical Conductivity
EIA	Environmental Impact Assessment
EMP	Environmental Management Program
EWR	Ecological Water Requirement
GA	General Authorisation
GMA	Groundwater Management Area
GMU	Groundwater Management Unit
GQM	Groundwater Quality Management
GRDM	Groundwater Resource Directed Measures
GRO	Gasoline Range Organics
GRU	Groundwater Resource Unit
На	Hectare
K	Hydraulic Conductivity
km	Kilometre
km²	Square Kilometre
l/h	litres/hour
I/s	litres/second
LDPE	Low density polyethylene
М	meter
m/d	Meters per day
m³	Cubic Meters



Term	Definition
m³/a	Cubic Meters/annum
m³/ha/a	Cubic Meters/hectare/annum
mamsl	meters above mean sea level
mbcl	meters below casing level
mbgl	meters below ground level
ML/d	Mega Litre/day
mm/a	Millimetres/annum
Mm³/a	Million Cubic Meters/annum
mS/m	Millisiemens per meter
NEMA	National Environmental Management Act
NGA	National Groundwater Archive
nm	not measured
NTU	Nephelometric Turbidity Units
NWA	National Water Act
°C	Degrees Centigrade
SABS	South African Bureau of Standards
SANAS	South African National Accreditation System
SANS	South African National Standards
SWL	Static water level
Т	Transmissivity
TMG	Table Mountain Group
тос	Total Organic Carbon
ТРН	Total Petroleum Hydrocarbons
WARMS	Water Use Authorization & Registration Management System
WRC	Water Research Commission
WULA	Water Use Licence Application



1 Introduction

Wisteria Boerdery (Pty) Ltd will be using groundwater for the irrigation of citrus orchards and other crops on the farms Buffels Hoek 180 (Portion 2) and Loerie River 436 (Portion 46), hereafter also referred to as the site. Groundwater will be abstracted from boreholes with volumes exceeding General Authorisation (GA) and therefore the water use needs to be licensed. Wisteria Boerdery (Pty) Ltd therefore appointed DHS Groundwater to conduct a geohydrological assessment as part of the Water Use License Application (WULA).

2 Geographical Setting

2.1 Site Location

The site is located on the Buffels Hoek 180 and Loerie River 436, located approximately 4km southwest of the town of Loerie, within the Eastern Cape Province. It covers an area of approximately 130 ha (Map 1, Appendix A).

2.2 Topography and Drainage

The site is located in quaternary catchment L90C within the Mzimvubu to Tsitsikamma Water Management Area (WMA). The site is drained by the Gamtoos River flowing in a south easterly direction. The topography on site can be described as follow:

- The northern portion of the site drains in a southern direction towards the Gamtoos River. The highest point of the water divide being ~160 mamsl.
- The southern portion of the site drains in a northernly direction towards the Gamtoos River. The highest point of the water divide being ~170 mamsl.
- Once the drainage has reached the lowest point within the central portion of the site (~4 mamsl), the site drains in a south easterly direction towards the sea in the Gamtoos River.

2.3 Climate

The weather is mild without extreme conditions with an average summer temperature of 21.59°C and a winter temperature of 14.39°C. The autumn months of March, April and May receive the lowest average windspeed of 11.03 km/h while the spring months of September, October and November receive the highest average windspeed of 14.08 km/h.

Meteorological data obtained from SamSam Water Climate Tool¹ is presented in Figure 1. Figures of 587 mm for the mean annual precipitation (MAP) and 1531 mm for the mean annual evaporation (MAE) is reported. The MAE exceeds the MAP by an order of magnitude, resulting in a negative moisture index. Rainfall within the study area is bimodal where both summer and winter rainfall occurs, a feature typical of the south-east coastal region of the country.

¹ https://www.worldclim.org/ & Global Aridity Index and Potential Evapotranspiration Climate Database v2



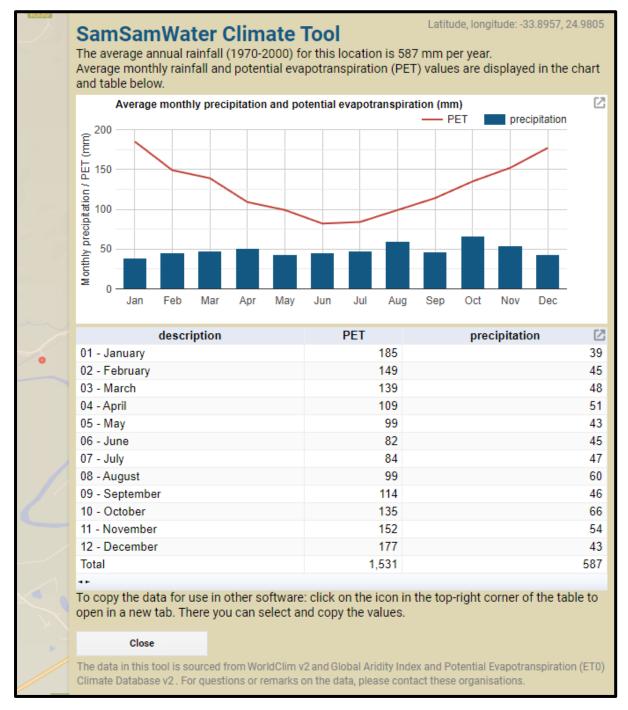


Figure 1. Precipitation and Evapotranspiration within the project area



3 Scope of Work

The objective of this assessment is to:

- Complete a geohydrological characterization of the groundwater in the vicinity of the site;
- Evaluate the proposed production boreholes in terms of yield and quality;
- Complete an assessment of the groundwater use in the area by means of a hydrocensus within the Groundwater Resource Unit as a minimum, up to a maximum distance of a 1km radius;
- Perform a Rapid Reserve Determination in support of a Water Use License Application (WULA) in terms of Section 21 of the National Water Act (NWA), 1998 (Act 36 of 1998)².
- Evaluate predicted impacts of groundwater abstraction on the receiving geohydrological environment;
- Propose measures to mitigate identified negative impacts;
- Develop a monitoring program as part of an environmental management plan;
- Document the above findings in a format fully compatible with the requirements for a WULA (Appendix 2) which is to be submitted to the Department of Water and Sanitation (DWS).

This report is not intended to be an exhaustive description of the assessment, but rather serves as a specialist geohydrological assessment to evaluate the overall geohydrological character of the site, to inform the impact assessment, and propose mitigation measures where applicable.

4 Methodology

It must be stated that no intrusive groundwater investigations (other than test pumping, groundwater level recording and sampling in existing borehole(s)) were done and reporting is thus based on and limited to observations made during the site visit, test pumping, hydrocensus and the collation of available information. The work completed for the purposes of compiling a geohydrological report comprised the following:

4.1 Desk Study

Undertake a desk study of existing information available from relevant literature, the National Groundwater Archive (NGA)³, the Water Use Authorization & Registration Management System (WARMS) and published geological and geohydrological maps and reports.

4.2 Site Visit & Hydrocensus

A site visit was conducted to evaluate the geology, geohydrology and potential receptors of possible groundwater impacts (quality and quantity) emanating from groundwater abstraction. A hydrocensus was carried out within the Groundwater Resource Unit as a minimum, up to a maximum distance of a 1km radius to identify legitimate groundwater users, the groundwater potential and quality. Where possible, groundwater levels were also measured to assist in the understanding of groundwater flow within the project area. Water samples were collected from selected boreholes and submitted for analysis of the major ions and trace elements.

² South African National Water Act (Act 36 of 1998)

³ http://www3.dwa.gov.za/NGANet/Security/WebLoginForm.aspx



4.3 Test Pumping

Seventy-two-hour constant discharge tests followed by recovery monitoring was conducted on the proposed production boreholes. Test pumping was conducted as per SANS 10299-4:2003 standards⁴. The data was scientifically analysed to calculate the sustainable yield of the tested boreholes. Water sample were collected and submitted to an SANAS accredited laboratory for the analysis of the major ions and trace elements.

4.4 Aquifer Vulnerability Assessment

The national scale groundwater vulnerability map, which was developed according to the DRASTIC methodology (DWAF, 2005)⁵ and recompiled in 2013 was used to assess the project area in terms of "Aquifer Vulnerability". Aquifer Vulnerability can be defined as "the likelihood for contamination to reach a specified position in the groundwater system after introduction at some location above the uppermost aquifer".

4.5 Water Balance & Reserve Determination

The "Reserve" and groundwater available for abstraction was calculated through a "Rapid Reserve Determination" using the "Groundwater Resources Directed Measures" software⁶ developed by the former Department of Water Affairs and Forestry (DWAF) as basis.

4.6 Aquifer Characterisation

The aquifer(s) underlying the project area was classified in accordance with "A South African Aquifer System Management Classification" developed by the Water Research Commission and DWAF.

4.7 Impact Assessment

The methodology to determine the significance of the potential impacts of groundwater abstraction was developed in 1995 and has been continually refined to date through the application of it to over 400 Environmental Impact Assessment (EIA) processes. The methodology is broadly consistent to that described in the Environmental Impact Assessment Regulations⁸ in terms of the NEMA⁹.

⁴ South African National Standard. Development, maintenance and management of groundwater resources. Part 4: Test-pumping of water boreholes (SANS 10299-4:2003, edition 1.1). ISBN 978-0-626-32920-4

⁵ DWAF, 2005. Groundwater Resources Assessment Project, Phase II (GRAII). Department of Water Affairs and Forestry, Pretoria.

⁶ "Groundwater Resources Directed Measures" Software (Version 4.0.0.0). Department of Water Affairs & Water Research Commission.

⁷ Department of Water Affairs and Forestry & Water Research Commission (1995). A South African Aquifer System Management Classification. WRC Report No. KV77/95.

⁸ Environmental Impact Assessment Regulations, 2014 published under Government Notice No. 982 in Government Gazette No. 38282 of 4 December 2014

⁹ National Environmental Management Act, 1998 (Act No. 107 of 1998) ("NEMA")



The risk associated with the groundwater abstraction for the property pertains to the operational phase only. Each impact was assessed individually and graded using a numerical system on the following factors:

- Duration
- Extent
- Intensity
- Probability

The values assigned to each factor were used to calculate the significance of each impact. Each individual impact was assessed and re-assessed after the appropriate mitigation was applied.

The "Impact Assessment Methodology" is presented in Appendix C.

4.8 Reporting

A technical report was compiled broadly consistent with applicable sections of the proposed geohydrology template presented in the "Regulations regarding the Procedural Requirements for Water Use Licence Applications and Appeals.¹⁰".

5 Regional and Local Geology

Based on the 1:250 000 Geological Series (3324 Port Elizabeth¹¹) the site is underlain by the Enon and Kirkwood Formations of the Uitenhage Group (Map 2, Appendix A). The Enon conglomerates are overlain by Kirkwood formation mudstone and sandstone and both overlain by river gravel terraces.

The lithostratigraphy is shown in Table 1.

Table 1. Lithostratigraphy of underlying geology

Group	Formation	Lithology		
Llitanhaga	Kirkwood (J-Kk)	Reddish & Greenish Mudstone, Sandstone.		
Uitenhage	Enon (Je)	Conglomerate, subordinate Sandstone, Mudstone.		
Quaternary		Alluvial & Fluvial sheet gravel and sand.		

¹⁰ Regulations regarding the Procedural Requirements for Water Use Licence Applications and Appeals. (Gazette No. 40713, GoR. 267, 24 March 2017)

¹¹ 1:250 000 Geological Map (3324 Port Elizabeth). Geological Survey, 1986.



6 Regional Geohydrology

Both the lithology and structural geology have a major bearing on the groundwater potential of the area. In their pristine state, the consolidated geological units have negligible groundwater potential. It is the secondary structural features that give the units groundwater potential. These secondary structures are usually associated with faults, fractures and weathering which gives rise to discrete zones of secondary permeability.

Unless otherwise stated, the published 1:500 000 General Hydrogeological Map¹² and associated explanatory booklet¹³ was used as basis to describe the regional geohydrological conditions.

6.1 Aquifer Types and Borehole Yields

The study area is underlain by both a shallow primary alluvial aquifer along the floodplain of the Gamtoos River and a deeper secondary fractured rock aquifer occurring within the conglomerates and sandstone of the Enon- and Kirkwood Formations.

The Uitenhage beds are described as a dense mass of rock with low permeability and limited groundwater potential. A borehole yield analysis indicates that close to 40% of successful boreholes yield less than 0.5 l/s. This does not account for unsuccessful boreholes which were destroyed or backfilled, which makes the success rate even worse.

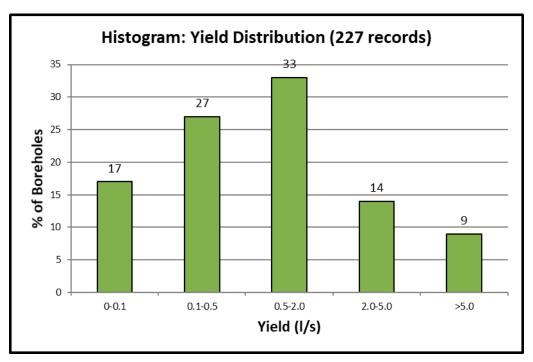


Figure 2. Yield Frequencies of borehole in the Uitenhage Group

Higher borehole yields are not uncommon, with yields of 2-5 l/s and >5 l/s (14% and 9% of borehole yields on record respectively) being reported, but this is not the norm.

^{12 1:500 000} General Hydrogeological Map, Port Elizabeth 3324 (1998)

¹³ MEYER, P S (1998). An explanation of the 1:500 000 General Hydrogeological Map Port Elizabeth 3324. Department of Water Affairs and Forestry, Pretoria.



Based on the 1:500 000 Hydrogeological Map, the primary alluvial aquifers within the buried gravel terraces of the Gamtoos River have a yield potential of 0.5-2.0 l/s, while the yield potential of the fractured rock aquifer within the Enon conglomerates and Kirkwood sandstone is reported to be as low as 0-0.1 l/s.

6.2 Depth to Groundwater

The static groundwater level generally occurs between 21 and 30m below surface¹⁴.

6.3 Groundwater Recharge and Baseflow

The study area falls within quaternary catchment L90C. The mean annual precipitation and annual recharge figures for the study area is presented in Table 2. Vegter's (1995)¹⁵ recharge and baseflow maps were used to obtain a first estimate of regional recharge and groundwater contribution to rivers and streams (baseflow).

Table 2. Regional Rainfall, Recharge and Baseflow

Mean Annual Precipitation (mm):	587
Annual Recharge (mm):	25 – 37
Percentage Recharge of MAP:	4.3% - 6.3%
Annual Baseflow (mm):	10 – 25
Percentage Baseflow of MAP:	1.7% - 4.3%

6.4 Groundwater Quality

Groundwater with Electrical Conductivity (EC) readings in the range of 150-370 mS/m is common. Sodium, calcium, magnesium, chloride and, occasionally sulphate often exceed maximum permissible drinking water limits (SANS 241-1:2015).

6.5 Aguifer Vulnerability

The national scale Groundwater Vulnerability Map, which was developed according to the DRASTIC methodology (DWAF, 2005) and recompiled in 2013 was used to assess the aquifers underlying the site in terms of "Aquifer Vulnerability". Aquifer Vulnerability can be defined as "the likelihood for contamination to reach a specified position in the groundwater system after introduction at some location above the uppermost aquifer".

The DRASTIC method takes into account the following factors:

- D = depth to groundwater (5)
- R = recharge (4)
- A = aquifer media (3)

¹⁴ DWA (Department of Water Affairs). (2005.). Groundwater Resource Assessment II

¹⁵ Vegter, J.R. (1995). An explanation of a set of national groundwater maps; WRC Report No. TT 74/95. Water Research Commission, Pretoria.



- S = soil type (2)
- T = topography (1)
- I = impact of the vadose zone (5)
- C = conductivity (hydraulic) (3)

The number indicated in parenthesis at the end of each factor description is the weighting or relative importance of that factor.

Aguifer Vulnerability is rated as follows:

Green represents the least vulnerable region that is only vulnerable to conservative pollutants in the long term when continuously discharged or leached

Yellow represents the moderately vulnerable region, which is vulnerable to some pollutants, but only when continuously discharged or leached.

Red represents the most vulnerable aquifer region, which is vulnerable to many pollutants except those strongly absorbed or readily transformed in many pollution scenarios.

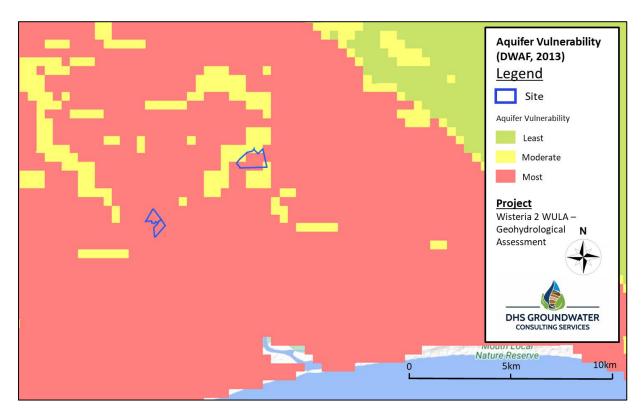


Figure 3. Regional groundwater vulnerability for the study area (DWAF, 2013).

The vulnerability of the aquifers within the project area is rated as "moderately to most vulnerable to pollutants".



7 Delineation of the Groundwater Resource Unit

A "Geohydrological Response Unit" (GRU), also referred to as a "Groundwater Resource Unit", is defined as a groundwater system that has been delineated or grouped into a single significant water resource based on one or more characteristics that are similar across that unit. Criteria to map a GRU would include:

- 1. Areas of similar geology;
- 2. Groundwater elevations generally mimic surface topography, and groundwater flows from higher lying ground towards lower lying springs or valleys (drainage lines), therefore surface water catchment boundaries may be used as surrogate for groundwater divides;
- 3. Rivers/Streams acting as a constant head boundary;
- 4. Impermeable dykes/lineaments acting as no-flow boundaries; and lastly
- 5. Expert judgement and interpretation.

For this study area there are clear drainage features that enable the definition of a more localised aquifer (i.e., a GRU). It is important to note that the Gamtoos River was not used as a boundary. The Gamtoos River can be considered as a gaining river being partially fed from the alluvial aquifer within the floodplain through which it flows. There is also a distinct difference in water quality from the alluvial aquifer (very high salinity) and the deeper fractured aquifer (low salinity) from which the production boreholes at the site draw water which strongly suggests that these two systems are not hydraulically linked. Boreholes on site were specifically constructed to seal of the alluvial aquifer containing inferior water quality.

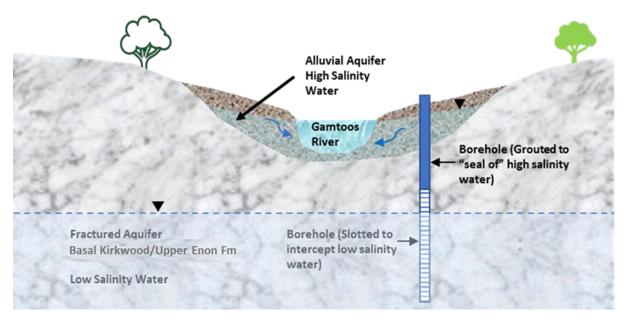


Figure 4. Conceptual model indicating the alluvial aquifer and deeper fractured aquifer

The GRU has been defined as follows:

- The northern, southern and western boundaries were defined by the topographic highs; and
- The eastern boundary was defined by topographic highs relating to the northern, southern and western boundaries.

The mapped GRU covers a total area of 2793 ha and is indicated on Maps 2 & 3, Appendix 1.



8 Site Specific Assessment

8.1 Existing Groundwater Information

8.1.1 National Groundwater Archive

A desktop hydrocensus was carried out within the GMU as a minimum, but it extended to at least a one-kilometre search radius around the site boundaries. This was done to determine groundwater use in the area. A search of the National Groundwater Archive (NGA), which provides data on borehole positions, groundwater chemistry and yield, when available, was carried out to identify proximal boreholes. These sites are then typically verified in the field and provide background information on the area, should they exist.

Under circumstances where the coordinate accuracy of most of the boreholes enumerated in the NGA is not better than 10 000 m, their positions are at least constrained to the boundaries of the topocadastral farms on which they are located. The associated geohydrological data and information therefore provides only a broad overview of groundwater conditions rather than site-specific information.

A search of the NGA produced three boreholes within a 1km radius from the site. The search radius was extended to a 5km radius and a further seven boreholes were identified. A summary of the data contained in the data base is presented in

Table 3. The regional locations of the boreholes were not plotted due to inaccurate and multiple duplicated coordinates.

Borehole yields extracted from the NGA data is slightly lower than the expected yields as given in the Port Elizabeth Hydrogeological Map (section 6.1). This can probably be attributed to the fact that boreholes were not necessarily drilled into the same geological formations and not scientifically sited. The median static water levels are in accordance with published regional data.

Table 3. Summary of data contained in the NGA

BH Id	Latitude	Longitude	Water Use	BH Depth (m)	SWL (mbgl)	Yield (L/s)
3324DD00012	-33.93212	24.97312		9.00	7.93	4.0700
3324DD00013	-33.93211	24.97312	Stock Watering	31.70	7.93	2.7100
3324DD00024	-33.92796	24.95924		82.30		
3324DD00090	-33.87101	24.99173		125.00	66.00	0.5400
3324DD00091	-33.87101	24.99174		90.00		
3324DD00092	-33.88767	24.99173		144.80	111.00	
3324DD00093	-33.88768	24.99175		155.00	91.00	0.3600
3324DD00143	-33.88545	24.97368		49.00	20.00	
3325CC00002	-33.87767	25.01621	Stock Watering	72.85	3.04	4.0700
3325CC00049	-33.85767	25.00482	Agriculture	60.61	24.24	2.3600
			n	10	8	7
			Min	9	3.04	0.06
			Max	155	111	4.07
			Median	77.575	22.12	2.36



8.1.2 Water Use Authorization & Registration Management System (WARMS)

WARMS data (updated 20 September 2022) was acquired for the study area to establish the volume of lawful groundwater use within the GRU. No registered groundwater users were listed within the delineated GRU. The closest registered groundwater users are located at a distance of more than 9.6km from the site.

8.2 Hydrocensus

A hydrocensus was conducted from 26 July 2022 to 27 July 2022 to establish groundwater use within the larger project area. The hydrocensus extended to a maximum distance of ~1km from the site boundaries, except where a river or a surface water body exist. The hydrocensus did not extend past such a feature as surface water bodies are usually hydraulically connected to an aquifer, act as a constant-head boundary and a groundwater pollution plume or cone of depression would theoretically not extend past a constant head boundary. Any information pertaining to the abstraction, yield and quality of groundwater was sought.

Apart from the five existing boreholes located within the site boundaries, an additional 12 boreholes were identified on neighbouring properties.

A summary of the most important data pertaining to the boreholes are summarised in Table 4. The borehole locations are presented in Map 4 in Appendix 1.

From the hydrocensus data it can be concluded that there is an increasing number of groundwater users within the GRU and where groundwater is abstracted, it is mainly used for agricultural purposes (irrigation watering).

The reported yields obtained from the hydrocensus are not in accordance with the Port Elizabeth Hydrogeological Map. As mentioned above, this could be due to boreholes drilled into different geological formations and/or not scientifically sited.

Apart from limited seasonal fluctuations in groundwater levels (<10%, based on previous experience in similar geology and rainfall), groundwater yields will remain consistent, irrespective of the season. The groundwater information can therefore be gathered indeterminate of the season.



Table 4. Details of boreholes located on neighbouring properties

BH nr	Coordinates Decimal Degrees (WGS84)	Depth (m)	Estimated Yield (I/s)	EC (mS/m)	Static water level (mbgl)	Equipment	Water Use	Property Owner (Cell nr.)
JFBH1	S -33.910634 E 024.943598	250	12.64	99	0	Submersible	Irrigation	Julian Ferreira (082 498
Josef 6	S -33.902730	147.9	5	272	27.55	Unequipped	~	0166) Lomon Ferreira
	E 024.947390							(071 175 3715) Lomon
Josef 5	S -33.903060 E 024.947140	149.1	1.94	146	26.35	Unequipped	~	Ferreira (071 175 3715)
Josef 4	S 33.745838 E 024.759844	148.9	~	203	25.59	Unequipped	~	Lomon Ferreira (071 175 3715)
PMBH1	S -33.869629 E 025.002186	303	2.08	105	0.93	Unequipped	~	Pierrie Moolman (072 047 5971)
ALBH1	S -33.876278 E 025.002399	300	11.11	75	1.94	Submersible	Irrigation	Ashley Ludwig (082 324 9316)
РМВН2	S -33.874544 E 024.995506	133.3	~	1830	4.03	Unequipped	~	Pierrie Moolman (072 047 5971)
JMBH1	S -33.887496 E 024.993290	303	1.94	73	~	Submersible	Irrigation	Jaco Muller (082 371 2735)



BH nr	Coordinates Decimal Degrees (WGS84)	Depth (m)	Estimated Yield (I/s)	EC (mS/m)	Static water level (mbgl)	Equipment	Water Use	Property Owner (Cell nr.)
DKBH1	S -33.897117 E 024.967512	180	3.61	330	10.08	Unequipped	Irrigation	Leon De Koning (082 822 3622)
DKBH2	S -33.896765 E 024.967242	180	~	1740	17.84	Unequipped	Irrigation	Leon De Koning (082 822 3622)
BJBH1	S -33.904292 E 024.957621	150	4.58	71.5	~	Solar	Irrigation/ Livestock	Bruce Johnson (082 653 4060)
BJBH2	S -33.903380 E 024.955706	150	1.39	239	14.5	Solar	Irrigation/ Livestock	Bruce Johnson (082 653 4060)





JFBH1 Josef 6







Josef 5 Josef 4





PMBH1 ALBH1







PMBH2 JMBH1





DKBH1 DKBH2







BJBH1

BJBH2

Figure 5. Borehole Photos on neighbouring properties

8.3 Groundwater Flow Direction

Generally, groundwater elevations mimic surface topography, and groundwater flows from higher lying ground towards lower lying springs or valleys (drainage lines). The general groundwater flow direction will thus initially be in a south-easterly direction along the Gamtoos River. The river changes course in the middle of the site and as such continues to flow in a north-easterly direction towards the Indian Ocean.

8.4 Pumptesting

Production boreholes were pumptested from April to October 2021. The pump tests were conducted by Welltek Services and the pumptesting data is attached in Appendix 4.

8.4.1 Description of a Pumptest

The efficient operation and utilization of a borehole require insight into and an awareness of its productivity and that of the groundwater resource from which it draws water. This activity, which is also known as pumptest, provides a means of identifying potential constraints on the performance of a borehole and on the exploitation of the groundwater resource.

The following tests were performed on the boreholes: (1) Step-Drawdown Test and (2) Constant Discharge Test.

8.4.1.1 Stepped Discharge Test

The purpose of the step drawdown test is to establish the efficiency of a single borehole and to provide preliminary information on the yield of the borehole (both from a quantitative and qualitative perspective). Often the insights gained from the step-test are used in the design and pumping rate of the constant discharge test.



8.4.1.2 Constant Discharge Test

A constant discharge test is performed to assess the productivity of the aquifer according to its response to the abstraction of water. This test entails pumping the borehole at a single pumping rate which is kept constant for an extended period. The test duration in this instance was 48 hours.

8.4.1.3 Recovery Monitoring

This test provides an indication of the ability of a borehole and groundwater system to recover from the stress of abstraction. This ability can again be analysed to provide information about the hydraulic properties of the groundwater system and arrive at an optimum yield for the medium to long term utilizations of the borehole.

8.4.2 Results & Data Interpretation

To estimate optimum pumping rates, pumping schedules and aquifer parameters, the pumptesting data were analysed by means of an Excel based software package developed by Van Tonder et al., (2002)¹⁶. In the software package, the Flow Characteristic method (FC-method), Cooper-Jacob-, FC Non-Linear- and Barker methods were used to estimate a risk-based sustainable yield for the borehole, as well as aquifer parameters such as transmissivity (T) and the storage coefficient (S).

The pumptesting data for the tested boreholes and FC-Solutions is presented in Appendix 4. The calculated sustainable yield for the boreholes together with the necessary information to equip the borehole is presented in Table 5.

Table 5. Management Recommendations for the tested boreholes

	Coordinates (WGS84)				WL (m)		Proposed	(m³)
Borehole nr.	S	E	Depth (m)	Static Water Level (m)	*Dynamic WL	Sustainable Yield (I/h) Pumping 24 hours/day	depth of pump installation (m)	Volume/day (m³)
MBH1	-33.906470°	24.955290°	108.26	19.04	75	6696	97	160.70
MBH2	-33.903260°	24.952220°	144	31.44	80	20916	120	501.98
SBH1	-33.912250°	24.953550°	248.4	4.1	60	37764	120	906.34
SBH2	-33.907500°	24.955833°	234.7	14.46	75	32580	135	781.92
вн3	-33.880178°	25.001164°	209	4.25	75	3276	160	78.62
						Total Volun	2429.57	
					7	0.887		

[#] Dynamic water level - Level at which the water level in the borehole stabilises after continuous pumping. To be used to calculate hydraulic heads when sizing submersible pumps.

The total volume of water which can be abstracted from the tested boreholes (0.887 Mm³/a) should never exceed the calculated water available for abstraction from the GRU. If the cumulative calculated

¹⁶ FC program for Aquifer Test Analysis (2013 version). Prof. Gerrit van Tonder, Fanie de Lange and Modreck Gomo. Institute for Groundwater Studies, University of the Free State.



sustainable yield of the tested borehole exceeds the water available for abstraction from the GRU, borehole yields or duty cycles need to be reduced.

8.5 Groundwater Quality

Groundwater samples were collected for analysis of the major ions and trace elements during pumptesting of the production boreholes. Four water samples were also collected from boreholes visited during the Hydrocensus (JFBH1, JMBH1, ALBH1 & BJBH1). The laboratory reports are presented in Appendix E.

Water quality results were compared with the SABS drinking water standards (SANS 241-1:2015, edition 2)¹⁷ (Table 6). Water is classified unfit for human consumption if the Standard Limits are exceeded. It must be emphasized that although the water use will mainly be used for irrigation purposes, it was compared to drinking water standards which is more stringent than irrigation standards.

Table 6. Water quality results compared to SANS 241-1:2015 (edition 2) drinking water standards

Sample Nr.	MBH1	MBH2	SBH1	SBH2	вн3	JFBH1	JMBH1	ALBH1	BJBH1	Standard Limits
рН	7.4	7.3	7.1	6.9	8.2	5.9	6.6	6.3	7.60	5.0 - 9.7
EC	105	85	97	80	99	108	61	83	81	170
TDS	681	550	608	520	644	691	390	530	518	1200
T-Alk						16	90			~
CI	218.0	181.0	226.0	191.0	225.0	255.0	100.0			300
SO₄	48.0	23.0	31.0	31.0	25.0	40.1	11.5			250
NO ₃ -N	0.00	0.22	0.00	0.00	0.00	0.00	0.00			11
NO ₂ -N	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.9
NH ₄ -N	0.00	0.10	0.00	0.00	0.00					1.5
F	0.20	0.30	0.30	0.30	0.70	0.42	0.24			1.5
Ca						12.90	8.52			~
Mg						21.00	16.30			~
Na	145.00	114.00	128.00	106.00	136.00	136.00	59.00			200
K						7.28	18.40			~
Al	0.00	0.00	0.00	0.00	0.02					0.3
Fe	0.31	0.99	0.69	4.10	0.41	0.07	0.39			0.3
Mn	0.15	0.08	0.41	0.58	0.00	1.42	0.06			0.1
В	0.24	0.20	0.26	0.00	0.14					2.4
Cr	0.00	0.00	0.00	0.00	0.00					0.05
Cu	0.00	0.00	0.00	0.00	0.00	0.00	0.23			2
Ni	0.00	0.00	0.00	0.00	0.00					0.07
Zn	0.00	0.00	0.00	0.00	0.00					5
Cd	0.00	0.00	0.00	0.00	0.00					0.003
Pb	0.00	0.00	0.00	0.00	0.00	0.00	0.01			0.01

Notes

Yellow = Acceptable

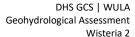
Exceeds standard limits

Blank = Not Analysed

0 = below detection limit of analytical technique

EC measurements in mS/m, other parameters in mg/ ℓ

¹⁷ SABS drinking water standards (SANS 241-1:2015) Second Edition. SABS Standards Division, March 2015. ISBN 978-0-626-29841-8





Within the site boundaries, the concentration of major elements (Cl, SO₄, NO₂, NO₃, F, Ca, Mg and Na) at boreholes MBH1, MBH2, SBH1, SBH2 and BH3 fall within the permissible limits for domestic use. However, the five boreholes within the site all have elevated Iron levels which exceed the SANS241 drinking water standard. Boreholes MBH1, SBH1 and SBH2 also have elevated levels of Manganese which renders this water unsafe for human consumption without prior treatment.

Boreholes JFBH1, JMBH1, ALBH1 and BJBH1 were sampled outside the site boundaries as part of the hydrocensus. Similarly, to the borehole water analysed within the site, the concentration of the major elements within boreholes JFBH1 and JMBH1 fall within the permissible limits for domestic use. The water in borehole JFBH1 has elevated Iron and borehole JMBH1 has elevated Manganese, emulating the elevated Iron and Manganese observed within the boreholes in the site.

The elevated levels of the constituents are likely contributed to the geological formation present and its chemical composition.

Of the nine sampled boreholes, none comply with the SANS241 Drinking Water Standards.

9 Reserve Determination & Water Balance

The sustainable volume of groundwater that can be abstracted from the aquifer(s) underlying the site was determined using data from the GRAII and WARMS datasets^{14, 18}. Associated information was collated from governmental and open-source datasets^{19, 20}. The reserve is taken into account when calculating the volume of water available for abstraction.

The site falls within quaternary catchment L90C and the default values, except where updated information was available, were used in the assessment in order to develop some guidance on the potential impact of the abstraction on the overall groundwater use in the catchment. It must be stated that the results achieved for the quaternary catchment is not necessarily applicable on the delineated Groundwater Resource Unit (GRU) due to compartmentalisation. Geological lineaments may act as no-flow boundaries while rivers/streams may act as constant head boundaries subdividing the quaternary catchments in smaller GRU's with different exploitation potentials. The results of the GRU should rather be considered when allocating a volume of groundwater for abstraction for this specific project.

¹⁸ Department of Water and Sanitation. Section 21(a) of the National Water Act, Taking Water From A Water Resource. DW760 Report. Accessed: 20 September 2022.

¹⁹ Department of Water and Sanitation. Notice 538 of 2016. National Water Act, 1998 (Act No. 36 of 1998). Revision of General Authorisation for the Taking and Storing of Water.

²⁰ https://wazimap.co.za/ Census Data.



9.1 Introduction

Definition of Reserve: "The quantity and quality of water required to supply basic needs of people to be supplied with water from that resource and to protect aquatic ecosystems in order to secure ecologically sustainable development and use of water resources".

To be able to quantify the groundwater component of the Reserve, the following relationship has to be solved:

$$GW_{allocate} = (Re + GW_{in} - GW_{out}) - BHN - GW_{Bf}$$

where: GW_{allocate} = groundwater allocation

Re = recharge

 GW_{in} = groundwater inflow GW_{out} = groundwater outflow BHN = basic human needs

GW_{Bf} = groundwater contribution to baseflow

Under the National Water Act (Act No. 36 of 1998) the water use must be authorised. The water will be abstracted from borehole(s), and used for commercial (agriculture/irrigation) purposes. Under these circumstances, the following (ground) water use is recognised as being relevant to the licence application:

Section 21 (a) – taking water from a resource.

9.2 Water Demand and Abstraction Classification

The calculated water demand for the project is 0.799 Mm³/annum. DWS categorises water use licence applications in three categories (presented in Appendix 2) based on the amount of recharge that is used by the applicant in relation to the specified property:

- Category A: Small scale abstractions (<60% recharge)
- Category B: Medium scale abstractions (60-100% recharge)
- Category C: Large scale abstractions (>100% recharge)

9.3 Assessment on Quaternary Level

The property falls within quaternary catchment L90C and the most salient parameters relevant to this catchment is presented in Table 7.

Table 7. Most salient parameters relevant to catchment L90C.

Area	Protected	GA	Recharge	Population ²⁰	Basic Human	EWR	Reserve	Current
km²	Area	(m³/ha/a) ¹⁹	(Mm³/a) ¹⁴		Need (Mm³/a)	Baseflow	(Mm³/a) ⁵	use
	(km²) ¹⁸					(Mm³/a)		(Mm³/a) ¹⁸
						5		
318	7.94	275	12.44	5018	0.046	2.51	2.556	0.367

It is assumed that General Authorisation as a possible route can be excluded.



9.3.1 Stress Classification

To provide a quantitative means of defining stress, a groundwater stress index was developed by dividing the volume of groundwater abstracted from a groundwater unit by the estimated recharge to that unit.

Stress Index = Abstraction/Recharge

= 0.367/12.44

= 0.029

The quaternary catchment is classified as Category A, which indicates "unstressed" levels of stress in terms of abstraction/recharge (Table 8).

Table 8. Guideline for determining the level of stress²¹

Present Status Category	Description	Stress Index (abstraction/recharge)
А	Unstressed or slightly stressed	<0.05
В	, ,	0.05 - 0.20
С	Moderately Stressed	0.20 - 0.40
D	,	0.40 - 0.65
E	Highly Stressed	0.65 – 0.95
F	Critically Stressed	>0.95

9.3.2 Reserve & Water available for allocation

The following table summarizes the reserve and water available for abstraction from the quaternary catchment.

²¹ Groundwater Resources Directed Measures Manual (WRC Report No TT299/07, April 2007)



Table 9. A summary of the Reserve for quaternary the catchment L90C.

Quantification of Reserve L90C						
Recharge:						
	Recharge [Mm³/a]	12.444				
Human Need:	7					
	Population	5018				
	Basic human need [I/d/p]	25				
minus -	Basic human need total [Mm³/a]	0.046				
Baseflow:						
	Baseflow [Mm³/a]	2.51				
	Maint. Low flow [Mm³/a]	0				
minus —	EWR [Mm³/a]	2.51				
Flow:						
minus -	Net Flow [Mm³/a]	0				
Reserve:						
	Reserve as % recharge	20.54				
equals -	Groundwater allocation [Mm³/a]	<u>9.888</u>				
	Current abstraction [Mm³/a]	<u>0.078</u>				

From Table 9 it becomes evident that the allocatable portion of the quaternary catchment far exceeds the current abstraction.



9.4 Assessment on Groundwater Resource Unit level

If the calculation is based on the GRU delineated for the project using the Groundwater Resources Assessment Project's (2005) range of recharge and baseflow figures, the following emerges:

Table 10. Water Balance within the Groundwater Resource Unit

Area	Surface Area (ha)	Groundwater to GRU using figure	recharge of
0.011	2793	12444800	
GRU	2793		m³/a/ha
		1093063.505	m³/a
	Recharge to GRU	2995	m ³ /day
		34.7	I/second
	Registered Use (WARMS)	0.0	m³/a
	Basic Human Need	4149.8	m³/a
RESERVE		2511180	m³/a
NESERVE	Base Flow (EWR)	79.0	m³/a/ha
		220564.3492	m³/a
		868349	m³/a
Groundwate	ur available for abstraction	0.868	Mm³/a
Giodilawate	Groundwater available for abstraction		I/day
		27.5	l/second
	Application (WULA)	0.799	Mm³/a
WULA as % of Gr	oundwater available in GRU	92.01	%

Based on the water balance results, the applied allocation of 0.799 Mm³/annum places the application in Category B abstraction (medium scale abstractions 60-100% recharge to the GRU) (see section 9.2). The tested boreholes will be able to supply 100% of the applied for volume.



10 Aquifer Classification

The aquifer(s) underlying the project area were classified in accordance with "A South African Aquifer System Management Classification, December 1995" by Parsons. Classification has been done in accordance with the following definitions for Aquifer System Management Classes:

- Sole Aquifer System: An aquifer which is used to supply 50% or more of domestic water for a
 given area, and for which there is no reasonably available alternative sources should the
 aquifer be impacted upon or depleted. Aquifer yields and natural water quality are
 immaterial.
- Major Aquifer System: Highly permeable formations, usually with a known or probable presence of significant fracturing. They may be highly productive and able to support large abstractions for public supply and other purposes. Water quality is generally very good (Electrical Conductivity of less than 150 mS/m).
- Minor Aquifer System: These can be fractured or potentially fractured rocks which do not have
 a high primary permeability, or other formations of variable permeability. Aquifer extent may
 be limited and water quality variable. Although these aquifers seldom produce large
 quantities of water, they are important for local supplies and in supplying base flow for rivers.
- Non-Aquifer System: These are formations with negligible permeability that are regarded as
 not containing groundwater in exploitable quantities. Water quality may also be such that it
 renders the aquifer unusable. However, groundwater flow through such rocks, although
 imperceptible, does take place, and needs to be considered when assessing the risk associated
 with persistent pollutants.

Based on the available information it can be concluded that aquifer system in the study area can be classified between a "Minor Aquifer System" and a "Major Aquifer System". The aquifers are productive and even used for Municipal supply.

In order to achieve an Aquifer System Management Index and a Groundwater Quality Management Index a point scoring system, as presented in Table 11 and Table 13 below, an intermediate aquifer system was inferred.

Table 11. Ratings for the Aquifer System Management and Second Variable Classifications:

Aquifer System Management Classification					
Class	Points	Study area			
Sole Source Aquifer System:	6				
Major Aquifer System:	4	3			
Minor Aquifer System:	2				
Non-Aquifer System:	0				
Special Aquifer System:	0 – 6				
Second Variable Classification					
(Weathering/Fracturing)					
Class	Points	Study area			
High:	3				
Medium:	2	2			
Low:	1				



The values in Table 11 are naturally subjective, but is based on the aquifer descriptions given previously. The importance of each aquifer should provide guidance on the protection to be assigned to each area.

The level of protection required of a groundwater system depend, amongst other, on the aquifer system classification class and the fractured extent and connectivity of the aquifers. The assumption is that a higher fracture presence results in a higher aquifer connectivity. An aquifer system management index can be derived with the following equation:

Aquifer System Management Index = Aquifer System Management Class x Fracturing

 $= 3 \times 2 = 6$

Table 12. Ratings for the Aquifer System Management Index

Aquifer System Management Index	Level of Protection	Study Area
<1	Limited	
1 - 3	Low Level	
3 - 6	Medium Level	
6 - 10	High Level	6
>10	Strictly Non-Degradation	

The ratings for the Aquifer System Management Classification and Second Variable Classification (Fracturing) yield an Aquifer System Management Index of 6 for the study area, indicating that a "high" level of groundwater protection is required in terms of prevailing groundwater flow regime management.

Table 13. Ratings for the Groundwater Quality Management (GQM) Classification System:

Aquifer System Management Classification					
Class	Points	Study area			
Sole Source Aquifer System:	6				
Major Aquifer System:	4	3			
Minor Aquifer System:	2				
Non-Aquifer System:	0				
Special Aquifer System:	0 - 6				
Aquifer Vulnerability Classification					
Class	Points	Study area			
High:	3				
Medium:	2	3			
Low:	1				

The vulnerability, or the tendency or likelihood for contamination to reach a specified position in the groundwater system after introduction at some location above the uppermost aquifer, in terms of the above, is classified as medium (section 6.5). The level of groundwater protection based on the Groundwater Quality Management Classification:

GQM Index = Aquifer System Management x Aquifer Vulnerability

 $= 3 \times 3 = 9$



Table 14. GQM index for the study area

GQM Index	Level of Protection	Study Area
<1	Limited	
1 - 3	Low Level	
3 - 6	Medium Level	
6 - 10	High Level	9
>10	Strictly Non-Degradation	

The ratings for the Aquifer System Management Classification and Aquifer Vulnerability Classification yield a Groundwater Quality Management Index of 9 for the study area, indicating that a "High" level of groundwater protection is required in terms of groundwater quality management.

In terms of DWS's overarching water quality management objectives which is (1) protection of human health and (2) the protection of the environment, the significance of this aquifer classification is that if any potential risk exists, measures must be triggered to limit the risk to the environment. In this instance it would be the (1) protection of the "Major Aquifer", (2) the external groundwater users in the area, and (3) maintain baseflow to the Gamtoos River which drains the subject area.



11 Impact Assessment

The risk associated with groundwater abstraction at the site pertains to the operational phase only. The most significant impacts considered as part of the impact assessment is listed below. Each impact was assessed individually and graded using a numerical system to calculate the significance of each impact. Each individual impact was assessed and re-assessed after the appropriate mitigation was applied. A compressive summary of the assessed impacts, mitigation and significance of each impact is listed in the tables below.

11.1.1 Depletion of the groundwater resource due to over-abstraction

Ref:		1			
Project phase	Operation				
Impact	Depletion of the groundwater resource due to over-abstraction				
Description of impact	over time. T	Over-abstraction of groundwater from boreholes is likely to lead to depletion of the water levels in the area over time. This can cause damage to the aquifer and might impact on neighbouring and registered groundwater users that are reliant on the same source of water. Reduced baseflow to streams/rivers and groundwater dependent eco systems (wetlands).			
Mitigatability	High	Mitigation exists and will considera	bly reduce the s	ignificance of impacts	
Potential mitigation	yield of bore	of boreholes as per "SANS 10299-4:21 holes. (2) Groundwater level monitor oundwater levels. (3) Take "Ecologica	ing - reduce abs		
Assessment		Without mitigation		With mitigation	
Nature	Negative		Negative		
Duration	Medium term	Impact will last between 5 and 10 years	Brief	Impact will not last longer than 1 year	
Extent	Local	Extending across the site and to nearby settlements	Very limited	Limited to specific isolated parts of the site	
Intensity	Moderate	Natural and/ or social functions and/ or processes are moderately altered	Very low	Natural and/ or social functions and/ or processes are slightly altered	
Probability	Probable The impact has occurred here elsewhere and could therefore occur		Probable	The impact has occurred here or elsewhere and could therefore occur	
Confidence	High	Substantive supportive data exists to verify the assessment	High	Substantive supportive data exists to verify the assessment	
Reversibility	Medium	The affected environment will only recover from the impact with significant intervention	High	The affected environmental will be able to recover from the impact	
Resource irreplaceability	Low	The resource is not damaged irreparably or is not scarce	Low	The resource is not damaged irreparably or is not scarce	
Significance		Minor - negative		Negligible - negative	
Comment on significance	After the implementation of mitigation measures, the significance of the impact becomes neglegible.				
Cumulative impacts	Since the impact is negligible negative with mitigation, cumulative impacts to groundwater with other projects are not anticipated.				



11.1.2 Groundwater quality deterioration as a result of over-abstraction

Ref:		2			
Project phase	Operation				
Impact	Groundwater quality deterioration as a result of over-abstraction				
Description of impact	adjacent geoh the area in go data acqu	Over-abstraction of groundwater from a borehole can potentially draw poorer water quality from the adjacent geohydrological environment into the borehole. This is likely to affect the groundwater quality in the area in general and might affect the supply in other boreholes within the fractured aquifer. Based on data acquired during the desk study and water quality results from boreholes sampled during the hydrocensus, it can be safely assumed that the water quality in the adjacent aquifers are of similar quality.			
Mitigatability	High	Mitigation exists and will considera	ably reduce the	significance of impacts	
Potential mitigation	Groundwa	ter level & quality monitoring - reduce groundwater levels and/or		9	
Assessment		Without mitigation		With mitigation	
Nature	Negative		Negative		
Duration	Short term	impact will last between 1 and 5 years	Brief	Impact will not last longer than 1 year	
Extent	Limited	Limited to the site and its immediate surroundings	Limited	Limited to the site and its immediate surroundings	
Intensity	Moderate	Natural and/ or social functions and/ or processes are moderately altered	Negligible	Natural and/or social functions and/or processes are negligibly altered	
Probability	Probable	The impact has occurred here or elsewhere and could therefore occur	Unlikely	Has not happened yet but could happen once in the lifetime of the project, therefore there is a possibility that the impact will occur	
Confidence	High	Substantive supportive data exists to verify the assessment	High	Substantive supportive data exists to verify the assessment	
Reversibility	Medium	The affected environment will only recover from the impact with significant intervention	Medium	The affected environment will only recover from the impact with significant intervention	
Resource irreplaceability	Low	The resource is not damaged irreparably or is not scarce	Low	The resource is not damaged irreparably or is not scarce	
Significance	Minor - negative			Negligible - negative	
Comment on significance	After the implementation of mitigation measures, the significance of the impact becomes neglegible.				
Cumulative impacts	Since the impact is negligible negative with mitigation, cumulative impacts to groundwater with other projects are not anticipated.				



12 Environmental Management & Groundwater Monitoring Program

The main objective of the proposed and discussed mitigation measures, pertaining to the identified impacts, is to maintain and monitor the regional groundwater table and quality to:

- Ensure that Schedule 1 water users within the catchment have adequate water supply to sustain the basic human need.
- Ensure that registered groundwater use within the catchment have adequate water supply.
- Ensure that adequate water is available to maintain groundwater dependent ecosystems (baseflow feeding the rivers/streams draining the subject area and wetlands).

A groundwater monitoring program was developed to reach the resource quality objectives. The onsite production boreholes need to be included in the network and are summarised in Table 15 below.

Table 15. Boreholes to be included in Monitoring Network

Borehole(s)	Objective
MBH1, MBH2, SBH1, SBH2 & BH3	Impact Monitoring

Table 16 below presents the parameters and frequency that should form part of the groundwater monitoring program. It is proposed that the data should be captured into an appropriate electronic database for easy retrieval and submission to the relevant authority as required, and reviewed by a geohydrologist on a bi-annual basis to ensure the source is utilised in a sustainable manner.

Table 16. Proposed Monitoring Requirements

Class	Parameter	Frequency	Motivation
Physical	Static groundwater levels	Monthly	Time dependant data is required to understand the regional groundwater flow dynamics. A lowering in the static water levels may indicate that the aquifer is utilised in an unsustainable way and abstraction rates need to be decreased. Conditions of the Water Use Licence.
	Groundwater abstraction volumes	Monthly	Calculate monthly & annual abstraction volumes. Conditions of the Water Use Licence.
Chemical	Major ions and trace elements.	Bi- annually	Changes in chemical and microbial composition may indicate areas of groundwater contamination and be used as an early warning system to implement management/remedial actions. To determine whether the water is fit for the intended use. Conditions of the Water Use Licence.



13 Conclusion & recommendations

Based on the field work, interpretation of available and newly acquired data, the abstraction of groundwater from the site will have an overall "negligible – negative" impact on the investigated geohydrological environment after implementation of appropriate mitigation measures. During the rating and ranking procedure of impacts, all identified impacts could be countered by appropriate mitigation.

Based on the water balance results, the applied allocation of 0.799 Mm³/annum places the application in a Category B abstraction (medium scale abstractions 60-100% recharge to the GRU). The tested boreholes will be able to supply in 100% of the demand, as well as the applied volume.

From a water quality point of view, elevated Iron and Manganese exceeding SANS241-1:2015 drinking water limits were reported in the boreholes located within the site as well as two other boreholes located outside the site sampled during the hydrocensus. Although the major elements are within the recommended drinking water limits, the elevated Iron and Manganese levels deem the groundwater unfit for human consumption.

It is the assessor's professional opinion that adequate information was available to appropriately assess the impact of groundwater abstraction from the production boreholes on the geohydrological environment. Based on the results, it is recommended that the application be approved. It is however imperative that the applicant implements the proposed "Environmental Management & Groundwater Monitoring Program". Production boreholes should be equipped as follow:

- Installation of a 32 mm LDPE observation pipe from the pump depth to the surface, open at the bottom. This allows for a 'window' of access down the borehole which enables manual water level monitoring and can house an electronic water level logger if required.
- Installation of a sampling tap (to monitor water quality).
- Installation of a flow volume meter (to monitor abstraction rates and volumes).
- The appropriate borehole pump must be installed, i.e., not an over-sized pump that is choked with a gate valve. If the monitoring shows that more water can be abstracted, then duty cycles (i.e., the duration of pumping time) may be increased, and not the flow rate.

<u>Disclaimer:</u> The calculated sustainable yield of the borehole(s) is based on data acquired during a short-term constant discharge test. The sustainable yield of a borehole may change for various reasons (lower than average rainfall, increased abstraction within the groundwater resource, mine dewatering, unknown geological boundary conditions, etc.). Continuous groundwater monitoring is critical to provide essential data needed to evaluate changes in the resource over time; as well as the long-term sustainability and status of an aquifer. In the event of anomalous groundwater level behaviour, abstraction rates and pumping cycles should be adapted until preoperational groundwater levels have been reached.



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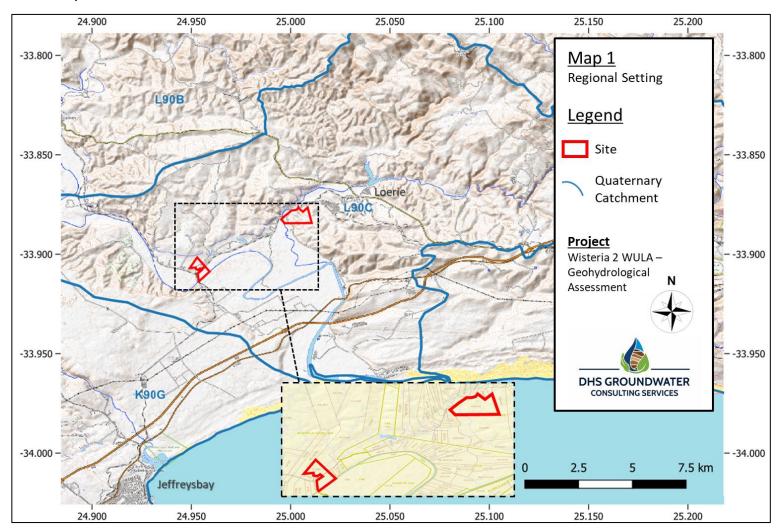
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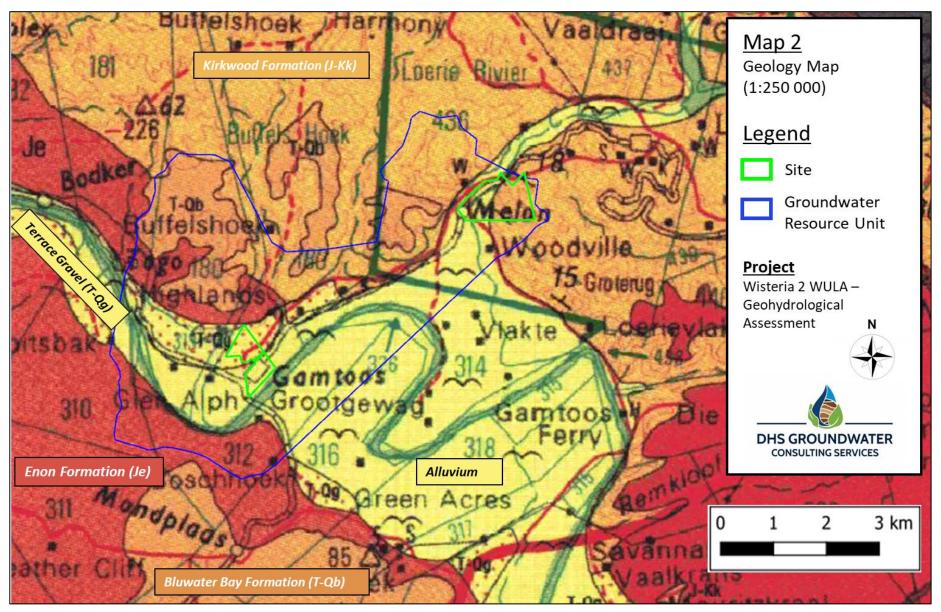


15 Appendices

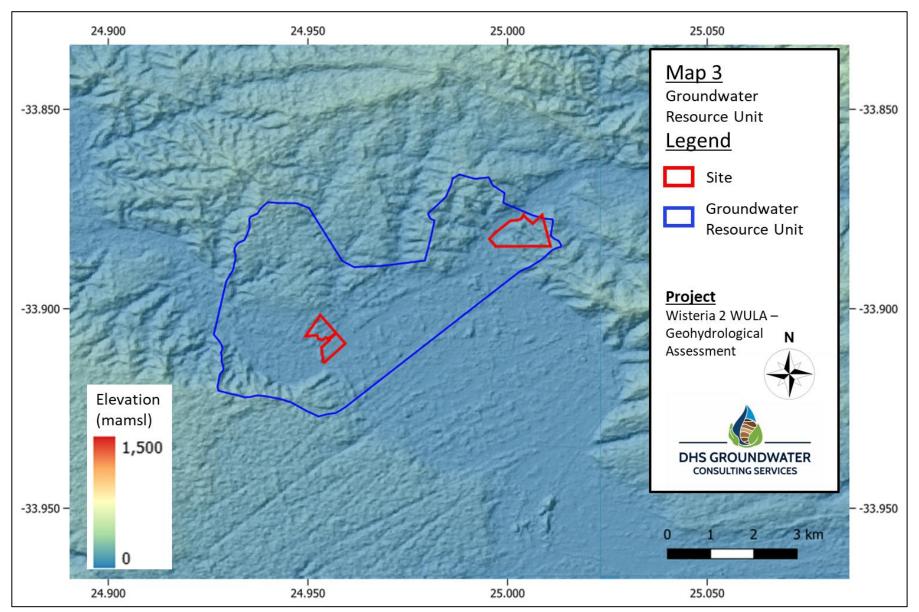
15.1 Appendix 1: Maps



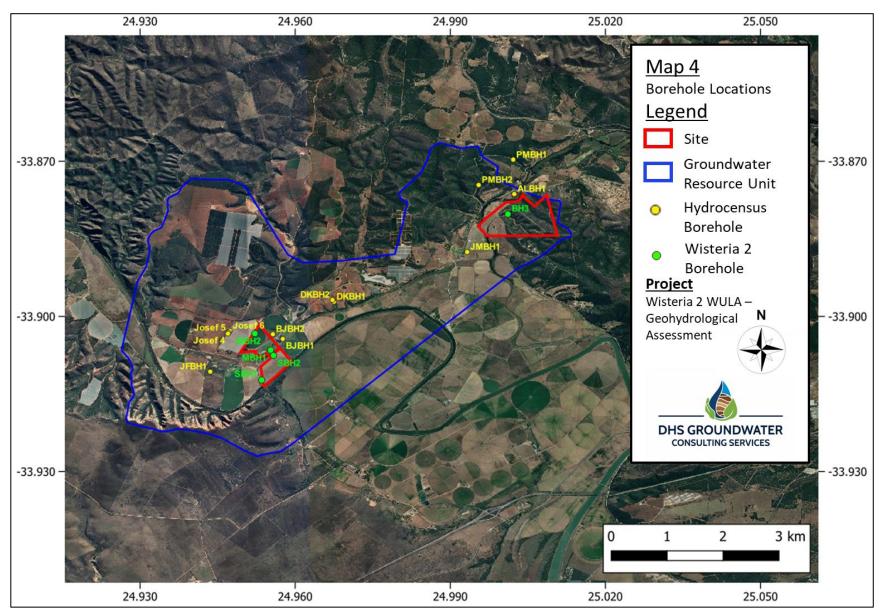














15.2 Appendix 2: DWS Guidelines for Water Use Licence Applications

ANNEXURE B

REQUIREMENTS FOR WATER USE LICENCE APPLICATION: GROUNDWATER ABSTRACTION [S 21 (a)]

The *Initial Regional* assessment is needed to determine the amount of information necessary for each new Water Use licence application for abstraction from groundwater, based on the amount of recharge that is used by the applicant in relation to the specified property.

Categories A, B and C list the information requirements for the licence application, as should be provided by the applicant to the Department of Water Affairs & Forestry.

Regional - Initial

- Size of property (AREAPROP)
- Recharge HP (RE)
- Existing use volume (ABS_{EX})
- New use volume (ABS_{NEW})
- Scale of abstractions (ABS_{SCALE})

CALCULATION

 $AREA_{PROP} * RE = RE_{AREA} (m^3/a)$

 $ABS_{EX} + ABS_{NEW} = ABS_{TOTAL} (m^3/a)$

ABSSCALE = (ABSTOTAL / REAREA) * 100

Please note: The calculation above should be

done for each proposed abstraction point (borehole), with the value of "AREA_{PROP}" being the area of the relevant aquifer within the property boundaries. The highest value for the relevant property should then be used to calculate the % of recharge as categorized below.

Small scale abstractions (<60% recharge on property)	Category A
Medium scale abstractions (60-100% recharge on property)	Category B
Large scale abstractions (>100% of recharge on property)	Category C

The Regional RDM support is info that should be submitted with the request for a Reserve determination. This will not only speed up the process, but also render more confidence to the Reserve determination.

Regional - RDM support

- Delineate resource units (default quaternary, unless geologically different)
- Delineate response units (same as resource unless existing information shows otherwise)
- Drainage (rivers and gauging stations in the resource unit area)
- Climate (average rainfall, reference source)
- Vegter regions (hydrological regions and recharge)
- Geo-hydrology wq, wl, aquifer tests, main fracture zones storage, sustainable yield, assurance of supply?
- Aquifer status: Local expert consideration (reference source), natural / impacted (mapping these areas in the resource unit), importance (both socio-economic and strategic), vulnerability, dependent ecosystems, total current use, classification (Parsons and current resource classification system).
- Licensing conditions wl, wq, level of acceptable degradation?
- Monitoring requirements according to the Category.
- Site visit necessary to validate all info regional and applicant



2

Category A

- Volume and purpose of the water required.
- Detail borehole census on the property in question. Information to be collected should include pump depth / borehole depth, depth to water level, yield of the borehole, volume abstracted (daily, weekly, monthly).
- Proximity to surface water discharges (springs, seeps, wetlands streams, rivers, lakes) and groundwater dependant ecosystems.
- Geo-referenced map of the property in question, with boreholes, physical structures (houses, stores, irrigation equipment) and current pollution sources (septic tanks, pit latrines, petrol/diesel tanks, irrigation areas) depicted.
- Monitoring programme monthly water levels, monthly rainfall.

Category B

- Geology of the area / borehole?
- Volume and purpose of the water required.
- Detail borehole census within a 1km width zone around the property in question as well
 as on the property itself. Information to be collected should at least include pump
 installation/borehole depth, depth to water level, yield of the borehole, volume abstracted
 (daily, weekly, monthly), water quality (one macro analysis per property).
- Proximity to surface water discharges (springs, seeps, wetlands streams, rivers, lakes) and groundwater dependant ecosystems.
- Geo-referenced map of the property in question, with boreholes, surface water features, physical structures (houses, stores, irrigation equipment) and current pollution sources (septic tanks, pit latrines, petrol/ diesel tanks irrigation areas) depicted.
- Contact details of relevant parties in the hydro census area.
- Potential impacts of potential use on groundwater and surface water quality.
- Monitoring programme weekly water levels, weekly rainfall, 6 monthly macro analysis
 and surface water discharges in the 1km width zone.

Category C

- A geo-hydrological report compiled by an acceptable and qualified geo-hydrological consultant. Report should include appropriate maps, tables and figures to support the conclusions and recommendations.
- Detail geology of the area, including structures, maps etc.
- Detail borehole census within at least 1km width zone around the area of recharge as well
 as on the area itself. Information to be collected for each borehole should at least include
 pump installation depth, borehole depth, depth of water level, yield of the borehole, depth
 of water strike(s), volume abstracted (daily, weekly, monthly) and water quality (one
 macro analysis per property in the zone).
- Aquifer description and characteristics including extent of the aquifer and hydraulic properties (storativity and transmissivity). This would require testing. Drilling might or might not be required. Groundwater piezometric contour map showing flow direction and a depth to water level contour map.



- Effective annual recharge on this property and the safe yield of the aquifer.
- Volume and purpose of the water required and the volume available for abstraction. A
 water balance that at least cover the <u>aquifer unit</u> in which the property is located should,
 in other words, is done that includes all gains and losses.
- Contact details of relevant parties in the hydro census area.

DHS GROUNDWATER

CONSULTING SERVICES

- Impact the abstraction will have on existing users and surrounding properties. This
 should be short- and long-term impact. This might have to be supported by a numerical
 model
- Proximity to and potential impact of the abstraction on surface water discharges and groundwater dependant terrestrial ecosystems.
- Potential impact of potential use on groundwater and surface water quality.
- Geo-referenced map of the property in question, with boreholes, surface water features, geological features, physical structures (houses, stores, irrigation equipment) and current pollution sources (septic tanks, pit latrines, petrol/diesel tanks, irrigation areas) depicted.
- Monitoring programme weekly water levels, weekly rainfall, 3 monthly macro analysis
 and surface water discharges and 6 monthly qualities in the 1km width zone.

The Department of Water Affairs and Forestry recommends that the following measures be taken when testing bore holes for sustainable yields and to provide the following information:

- Refer to test procedures in the South African National Standards Code No.: SANS 10299.
- Perform a three (3) hour stepped draw down test to determine the discharge rate of the intended constant rate test OR;
- The constant discharge test should be done at approximately ²/₃ of the blow yield of the bore hole.
- For HOUSEHOLD use it as recommended that a 8 hour constant rate test be performed with the draw down and the recovery measured.
- For IRRIGATION it as recommended that a 24 constant rate test should be performed while the draw down and the recovery is measured. This test could also be performed for intended BULK WATER SUPPLY for a volume of up to 150 000 m³ per annum.
- For BULK WATER SUPPLY in excess of 150 000 m³ per annum it as recommended that a 72 hour constant rate test should be performed while the draw down and the recovery of the bore hole is measured.
- All data as obtained above should be attached to the relevant Water Use License Application forms, together with an analysis of the data (including draw down curves) and recommendation for the sustainable yield of the borehole(s), by a qualified Geohydrologist.

NOTE: The above-recommended requirements may change without prior notice as required by DWAF to effectively manage the respective water resource.



15.3 Appendix 3: Impact Assessment Methodology

METHODOLOGY FOR THE ASSESSMENT OF IMPACTS

The assessment of the predicted significance of impacts for a proposed development is by its nature, inherently uncertain – environmental assessment is thus an imprecise science. To deal with such uncertainty in a comparable manner, a standardised and internationally recognised methodology has been developed. This methodology will be applied in this study to assess the significance of the potential environmental impacts of the proposed development.

For each predicted impact, certain criteria are applied to establish the likely **significance** of the impact, firstly in the case of no mitigation being applied and then with the most effective mitigation measure(s) in place.

These criteria include the **intensity** (size or degree scale), which also includes the **type** of impact, being either a positive or negative impact; the **duration** (temporal scale); and the **extent** (spatial scale). For each predicted impact, the specialist applies professional judgement in ascribing a numerical rating for each of these criteria respectively as per Table 1, Table 2 and Table 3 below. These numerical ratings are used in an equation whereby the **consequence** of the impact can be calculated. Consequence is calculated as follows:

Consequence = type x (intensity + duration + extent)

Depending on the numerical result, the impact's consequence would be defined as either extremely, highly, moderately or slightly detrimental; or neutral; or slightly, moderately, highly or extremely beneficial. These categories are provided in Table 5 and Table 6.

To calculate the significance of an impact, the **probability** (or likelihood) of that impact occurring is also taken into account. The most suitable numerical rating for probability is selected from Table 4 below and applied with the consequence as per the equation below:

Significance = consequence x probability

Depending on the numerical result, the impact would fall into a significance category as negligible, minor, moderate or major, and the type would be either positive or negative. These categories are provided in Table 6.

Once the significance of an impact occurring without mitigation has been calculated, the specialist must also apply their professional judgement to assign ratings for the same impact after the proposed mitigation has been implemented.

The tables on the following pages show the scales used to classify the above variables, and define each of the rating categories.



Table 1 | Definition of Intensity ratings

	Criteria		
Rating	Negative impacts (Type of impact = -1)	Positive impacts (Type of impact = +1)	
7	Irreparable damage to biophysical and / or social systems. Irreplaceable loss of species.	Noticeable, on-going benefits to which have improved the quality and extent of biophysical and / or social systems, including formal protection.	
6	Irreparable damage to biophysical and / or social systems and the contravention of legislated standards.	Great improvement to ecosystem processes and services.	
5	Very serious impacts and irreparable damage to components of biophysical and / or social systems.	On-going and widespread positive benefits to biophysical and / or social systems.	
4	On-going damage to biophysical and / or social system components and species.	Average to intense positive benefits for biophysical and / or social systems.	
3	Damage to biophysical and / or social system components and species.	Average, on-going positive benefits for biophysical and / or social systems.	
2	Minor damage to biophysical and / or social system components and species. Likely to recover over time. Ecosystem processes not affected.	Low positive impacts on biophysical and / or social systems.	
1	Negligible damage to individual components of biophysical and / or social systems.	Some low-level benefits to degraded biophysical and / or social systems.	

^{*}NOTE: Where applicable, the intensity of the impact is related to a relevant standard or threshold, or is based on specialist knowledge and understanding of that particular field.

Table 2 | Definition of Duration ratings

Rating	Criteria Criteria
7	Permanent: The impact will remain long after the life of the project
6	Beyond project life: The impact will remain for some time after the life of the project
5	Project Life: The impact will cease after the operational life span of the project
4	Long term: 6-15 years
3	Medium term: 1-5 years
2	Short term: Less than 1 year
1	Immediate: Less than 1 month



Table 3 | Definition of Extent ratings

Rating	Criteria
7	International: The effect will occur across international borders
6	National: Will affect the entire country
5	Province/ Region: Will affect the entire province or region
4	Municipal Area: Will affect the whole municipal area
3	Local: Extending across the site and to nearby settlements
2	Limited: Limited to the site and its immediate surroundings
1	Very limited: Limited to specific isolated parts of the site

Table 4 | Definition of Probability ratings

Rating	Criteria
7	Certain/ Definite: There are sound scientific reasons to expect that the impact will definitely occur
6	Almost certain/Highly probable: It is most likely that the impact will occur
5	Likely: The impact may occur
4	Probable: Has occurred here or elsewhere and could therefore occur
3	Unlikely: Has not happened yet but could happen once in the lifetime of the project, therefore there is a possibility that the impact will occur
2	Rare/ improbable: Conceivable, but only in extreme circumstances and/ or has not happened during lifetime of the project but has happened elsewhere. The possibility of the impact manifesting is very low as a result of design, historic experience or implementation of adequate mitigation measures
1	Highly unlikely/None: Expected never to happen.



Table 5 | Application of Consequence ratings

Range		Significance rating
-21	-18	Extremely detrimental
-17	-14	Highly detrimental
-13	-10	Moderately detrimental
-9	-6	Slightly detrimental
-5	5	Negligible
6	9	Slightly beneficial
10	13	Moderately beneficial
14	17	Highly beneficial
18	21	Extremely beneficial

Table 6 | Application of significance ratings

Range		Significance rating	
-147	-109	Major - negative	
-108	-73	Moderate - negative	
-72	-36	Minor - negative	
-35	-1	Negligible - negative	
0	0	Neutral	
1	35	Negligible - positive	
36	72	Minor - positive	
73	108	Moderate - positive	
109	147	Major - positive	

Despite attempts at providing a completely objective and impartial assessment of the environmental implications of development activities, environmental assessment processes can never escape the subjectivity inherent in attempting to define significance. The determination of the significance of an impact depends on both the context (spatial scale and temporal duration) and intensity of that impact. Since the rationalisation of context and intensity will ultimately be prejudiced by the observer, there can be no wholly objective measure by which to judge the components of significance, let alone how they are integrated into a single comparable measure.



This notwithstanding, in order to facilitate informed decision-making, environmental assessments must endeavour to come to terms with the significance of the potential environmental impacts associated with particular development activities. Recognising this, Geovation has attempted to address potential subjectivity in the current EIA process as follows:

- Being explicit about the difficulty of being completely objective in the determination of significance, as outlined above;
- Developing an explicit methodology for assigning significance to impacts and outlining this methodology in detail. Having an explicit methodology not only forces the specialist to come to terms with the various facets contributing towards the determination of significance, thereby avoiding arbitrary assignment, but also provides the reader with a clear summary of how the specialist derived the assigned significance;
- Wherever possible, differentiating between the likely significance of potential environmental impacts as experienced by the various affected parties; and
- Utilising a team approach and internal review of the assessment to facilitate a more rigorous and defendable system.

Although these measures may not totally eliminate subjectivity, they provide an explicit context within which to review the assessment of impacts.



15.4 Appendix 4: FC Solutions & Pumptesting Data Sheets

Summary		Wisteria 2 - Magalies Farm BH1									
Method	Sustainable yield (I/s)	Std. Dev	Early	T (m²/d)	Late T (m²/d)	S	AD used			
Basic FC	1.63	0.91		6	3.0)	2.20E-03	70.1	1.627		
Advanced FC											
FC inflection point											
Cooper-Jacob	2.05	1.33			5.8	,	2.75E-03	70.1	2.048		
FC Non-Linear											
Barker	1.89	1.25	K _f =	88		S _s =	1.00E-07	70.1	1.891		
Average Q_sust (I/s)	1.86	0.21	b =	0.10	Fractal dimension r	1 =	1.95				
December de d'ale	-44:4 (1 /-)					_	1				
		1				day					
		2.63	9468	Vhr			4				
	Method Basic FC Advanced FC FC inflection point Cooper-Jacob FC Non-Linear Barker Average Q_sust (I/s) Recommended about the substitution of the s	Method Sustainable yield (I/s) Basic FC 1.63 Advanced FC FC inflection point Cooper-Jacob 2.05 FC Non-Linear Barker 1.89 Average Q_sust (I/s) 1.86 Recommended abstraction rate (L/s) Hours per day of pumping (L/s) 12	Method Sustainable yield (I/s) Std. Dev Basic FC 1.63 0.91 Advanced FC	Method Sustainable yield (I/s) Std. Dev Early Basic FC 1.63 0.91 Advanced FC	Method Sustainable yield (I/s) Std. Dev Early T (m²/d) Basic FC 1.63 0.91 6 Advanced FC 5 1.33 5 FC inflection point 1.33 1.33 1.33 FC Non-Linear 1.89 1.25 K₂ = 88 Average Q_sust (I/s) 1.86 0.21 b = 0.10 Recommended abstraction rate (L/s) 1.86 6696 I/hr Hours per day of pumping (L/s) 12 2.63 9468 I/hr	Method Sustainable yield (I/s) Std. Dev Early T (m²/d) Late T (Basic FC 1.63 0.91 6 3.0 Advanced FC FC inflection point Cooper-Jacob 2.05 1.33 5.8 FC Non-Linear Barker 1.89 1.25 K _f = 88 Average Q_sust (I/s) 1.86 0.21 b = 0.10 Fractal dimension rowspan="2">Fractal dimension rowspan="2">Fractal dimension rowspan="2">Fractal dimension rowspan="2">Fractal dimension rowspan="2">Fractal dimension rowspan="2">Barker 1.86 6696 Whr For 24 hrs per Hours per day of pum ping (L/s) 12 2.63 9468 Whr 12 hrs per day	Method Sustainable yield (I/s) Std. Dev Early T (m²/d) Late T (m²/d) Basic FC 1.63 0.91 6 3.0 Advanced FC FC inflection point Cooper-Jacob 2.05 1.33 5.8 FC Non-Linear Barker 1.89 1.25 K _f = 88 S _s = Average Q_sust (I/s) 1.86 0.21 b = 0.10 Fractal dimension n = Recommended abstraction rate (L/s) 1.86 6696 I/hr For 24 hrs per day Hours per day of pumping (L/s) 12 2.63 9468 I/hr 12 hrs per day	Method Sustainable yield (I/s) Std. Dev Early T (m²/d) Late T (m²/d) S Basic FC 1.63 0.91 6 3.0 2.20E-03 Advanced FC FC inflection point Cooper-Jacob 2.05 1.33 5.8 2.75E-03 FC Non-Linear Barker 1.89 1.25 K _f = 88 S _s = 1.00E-07 Average Q_sust (I/s) 1.86 0.21 b = 0.10 Fractal dimension n = 1.95 Recommended abstraction rate (L/s) 1.86 6696 I/hr For 24 hrs per day Hours per day of pumping (L/s) 12 2.63 9468 I/hr 12 hrs per day	Method Sustainable yield (I/s) Std. Dev Early T (m²/d) Late T (m²/d) S AD used Basic FC 1.63 0.91 6 3.0 2.20E-03 70.1 Advanced FC FC inflection point Cooper-Jacob 2.05 1.33 5.8 2.75E-03 70.1 FC Non-Linear Barker 1.89 1.25 K _f = 88 S _s = 1.00E-07 70.1 Average Q_sust (I/s) 1.86 0.21 b = 0.10 Fractal dimension n = 1.95 Recommended abstraction rate (L/s) 1.86 6696 I/hr For 24 hrs per day Hours per day of pumping (L/s) 12 2.63 9468 I/hr 12 hrs per day		

Amount of water allowed to be abstracted per month	4821.12	m ³
Borehole could satisfy the basic human need of	6428	persons
Is the water suitable for domestic use (Yes/No)		

Recommended pump depth below surface (m)	97	
Total Casing length	108.26	
Blow yield (I/s)		
Expected dynamic water level over 24hr pump	75	mbcl
Critical depth that water level must not exceeded	97	mbcl
Depth of BH	108.26	mbcl
Static Water Level	19.04	mbcl

metres below casing level

8 hrs per day



9 Schubert Road Walmer Heights Port-Elizabeth 6070 South Africa

T +27 (0) 82 099 2366 E divan@dhsgroundwater.co.za W https://dhsgroundwater.co.za

Divan Stroebel (Pr.Sci.Nat, MGSSA)

Hydrogeologist - Director

DHS Groundwater Consulting Services

15/10/2021

Management recommendations

The aquifer consists of a good fracture network with radial flow present. Transmissivity is in the order of 3.0 to 6 m2/day.

An available drawdown of 97 mbcl is recommended.

Hours per day of pumping (L/s)

As a rule of thumb, 60% of the total available drawdown (depth between main water strike and static water level) can be utilised without jeopardizing aquifer sustainability.

A dynamic water level of 75 mbcl is anticipated over a 24hr pump schedule at a volume of 1.86 l/s.

The water level should not exceed 97 mbcl, which is referred to as the critical water level.

Consistent drawdown below the critical water level will have a negative impact on the aquifer sustainability and yield.

It is therefore HIGHLY recommended to monitor the water level closely during pumping, to prevent drawdown in excess of 97 mbcl.

A conduit should be installed alongside the pump to allow for the measurement of the water level.

A CALIBRATED FLOW METER MUST BE INSTALLED AT THE IMMEDIATE PUMP OUTLET AT THE BOREHOLE TO ENSURE THE RECOMMENDED PUMP VOLUMES ARE NOT EXCEEDED.

PLEASE NOTE: Borehole is in close proximity to neighbouring boreholes. It is therefore of utmost importance to monitor water levels during abstraction within all boreholes.



Scenic route 565 t/a Welltek Services Vat nr: 45902 54720 Email: welltekservices@gmail.com



Borehole testing and associated projects

CC Registration nr: 2005/137492/23 18 Highfield Road, EAST LONDON, 5205 Cell: +27 (0)71 031 5086 Fax: +27 (0)86 517 9242

		В	OREHOLE TEST RECORD	
Borehole Number:	BH 4 ONDER H	UIS LOERIE	Province:	EASTERN CAPE
Alternative Number:			District:	LOERIE
Coordinates: Latitude [°S]	33,906470		Town/Village/Farm:	ONDER HUIS
Longitude [°E]	24,955290		Rig Type & number:	ISUZU
Date & Time Test Started:	2021/10/10 00	0:00	Operator:	ELISHA
Date & Time Test Ended:	2021/10/20 00	0:00	Supervisor:	HERMAN
Consultant:	DHS			
CONSULTANT - DATA PR	OVIDED / INST	RUCTIONS:		EXISTING INSTALLATION:
Borehole	e depth [mbgl]:		Diesel/Electric/Wind/Hand	ELECTRIC
В	Blow Yield [I/s]:		Pump Make & Serial no:	CRI
Water Strike D	epth(s) [mbgl]:		Intallation Depth (m)	97,94 M
Installation	n depth [mbgl]:		Type & Condition - Pump:	SUBMERSIBLE WORKING
Estimated Step	s [I/s] - Step 1:		- Column:	HDPE PIPE
	Step 2:		- Pump House	N/A
	Step 3:			FIELD MEASUREMENTS:
	Step 4:		Depth Before Test [mbcl]:	108,26
	Step 5:		Depth after Test [mbcl]:	108,26
	Step 6:		Water Level before Test [mbcl]:	19,04
Step	Duration [min]:		Water Level after Test [mbcl]:	25,98
Step Recovery	Duration [Hrs]:		Casing Depth [mbcl]:	PVC
Cons	tant Yield [l/s]:		Casing Height [magl]:	0,38
Constant	Duration [Hrs]:		Casing Diameter [mm]:	140,00
Recovery Duration [Hrs] /	Drawdown %:			TEST PUMP INSTALLATION DETAILS:
Lenghth of Layfla	t Required [m]:		Pump Used:	BP 30 M
Frequency of pH and EC	Measurements:		Depth Installed [mbcl]:	98,00
SAMPLE IN	STRUCTIONS:		Datum Level above Casing [m]:	0,25
			Length of Layflat [m]:	100,00
			GENERAL ACTIONS:	
Supplied new steel of	over [Yes/No]:	NO	Slug Test [Yes/No]:	N/A
Velded existing steel cover	back on [Y/N]:	NO	Re-install existing pump	P [Yes/No]: YES LEFT IT WORKING
Borehole Mai	rking [Yes/No]:	NO	If not, where was it stored?	N/A
Site Cleaning and Finis	shing [Yes/No]:	YES	Maintenance work [Hrs]:	N/A
Data Reporting and Recor	rding [Yes/No]:	YES	Maintenance Travel [km]:	N/A
Digital Photo Ta	aken? [Yes/No]	NO	List of parts replaced/repaired:	N/A
RETREAT	FROM SITE		Date &Time Sampled:	NO SAMPLE TAKEN
It is hereby acknowledged that existing equipment is in an ac			COM	IMENTS BY ONSITE CREW
NAME:				
DESIGNATION:				
SIGNATURE:			***************************************	
DATE:				
1	L			



BOREHO	LE NO: 4 ON	DER HUIS	LOEF W	VATER LEVEL			19,29	W	ATER DEP	TH [mbgl]:	18,66	AVA	ILABL	LE DRAWI	DOWN [m]	: 78,96
DIC	CITA DOD DAG	TD 1	DDM						1	RECOVER	Y	DICCULARC	T D A	(TST) ()	DDM	
	CHARGE RAT		RPM 21/10/10 1	4.50		DISCHAR TE & TIME	GE RA		RPM 1/10/10 15:	F.C.	_	DISCHARG ATE & TIME	ERA	TE 3	RPM	140 46.E6
TIME	DRAWDOWN	YIELD	TIME	RECOVER			VDOWN	YIELD	TIME	RECOVE			OW/N	YIELD	TIME	/10 16:56 RECOVERY
(min)	(m)	(I/s)	(min)	(m)	(min		m)	(I/s)	(min)	(m)	(mir			(l/s)	(min)	(m)
1	2,04	` ,	1	. ,	1	8	,73		1	, ,	1	13, 1	4	, ,	1	
2	2,87		2		2		,21		2		2	15,3			2	
3	3,62		3		3		,65	3,36	3		3	16,5		5,21	3	
5 7	4,51	1.00	5 7		5 7		0,01		5 7		5 7	17,6			5 7	
10	5,39	1,68	10		10), 30), 54	3,38	10		10	18,4		5,23	10	
15	6, 10 6, 58		15		15		0,71	0,00	15		15	20,9		0,20	15	
20	6,97	1,67	20		20		0,86	3,37	20		20	21,4			20	
30	7,56		30		30	13	L,09		30		30	22,6	32	5,20	30	
40	7,90	1,68	40		40		1,33	3,35	40		40	23,8			40	
50	8, 14		50		50		L,54		50		50	24,5		5, 22	50	
60	8,40		60 70		60	1.	L,70		60 70		60	25,0	10		60 70	
			80		+				80						80	
			90						90						90	
			100						100						100	
			110						110						110	
			120						120						120	
			150						150						150	
Av	erage Yield (I/s): Drawdown (%):		180			Average Yi	eld (l/s): own (%):		180 210			Average Yield Drawdowr	, ,	5,21 31,66	180 210	
DIC	CHARGE RA		210 RPM		+	DISCHAR			RPM		-	DISCHARG	• •		RPM	
	& TIME		21/10/10 1	7:56		TE & TIME	GE IGI		1/10/10 17:	56	n	ATE & TIME	L 101	IID U		/10 17:56
TIME	DRAWDOWN	YIELD	TIME	RECOVER			VDOWN	YIELD	TIME	RECOVE			OWN	YIELD	TIME	RECOVERY
(min)	(m)	(I/s)	(min)	(m)	(min		m)	(I/s)	(min)	(m)	(mir		-	(l/s)	(min)	(m)
1	26,73	` '	1	, ,	1	, <u> </u>	,	` '	1	. ,	1	, , ,		. ,	1	41,63
2	27,87		2		2				2		2				2	36,20
3	29,48		3		3				3		3				3	31,02
5	30,69	8,05	5		5				5		5				5	26, 19
7 10	31,80 33,30	8,04	7 10		7				7		7 10				7	19,82 14,53
15	35,63	0,04	15		15				15		15				15	9,29
20	37,1	8,03	20		20				20		20				20	7,03
30	39,44		30		30				30		30				30	5,84
40	43,63	8,02	40		40				40		40				40	5,42
50	45,82		50		50				50		50				50	5, 10
60	48,06		60 70		60				60 70		60				60 70	4,73
			80		+				80		+				80	4,52 4,37
			90						90						90	4,26
			100						100						100	3,95
			110						110						110	3,74
			120						120						120	3,56
			150	-	_				150						150	3,38
			180 210	-	+				180 210						180 210	3,17 2,88
			240	 	+				240		-				240	2,88
Av	erage Yield (I/s):	8,03	300			Average Yi	eld (l/s):	0,00	300			Average Yield	(l/s):	0,00	300	2,29
	Drawdown (%):		360				own (%):		360			Drawdow	` '		360	2,18
	EVEL ABOVE GR									D PUMPED ?		-				
STATIC V	VATER LEVEL AF	TER STEP	PED DISC	HARGE TEST	[mbdl]:	19,29			WAS THE	WATER CLE	EAN? YES					
						Cata	ת עמפו	R VIXID∪	WN SUM	MAPV						
	DURATION	DRAWDO	WN	AVERAGE	ı	RECOVERY	ע עניי		DURATION		OOWN	AVERAGE			RECOVE	RY
STEP		m]	[%]	YIELD [I/s]	[min]	[m]	[%]	STEP	[min]	[m]	[%]	YIELD [I/s]	[mir	n]	[m]	[%]
1			10,64	1,68				5		0,00		0,00				
2			14,82	3,36				6		0,00		0,00				
3 4		-	31,66 60.87	5,21 8,03				7								
	TIME END:	,	60,87 2021/10/1					TOTAL:	240,00	48,06	60,87		0		0.00	0,00
COMME								· • // L	0,00	,	20,01	1			-,	3,00
						ABLISHMENT							BLISHMENT DATE:		2021/10/10	
	MOVE	BOREHO	DLE		AGE	MOV		BOREH			LAGE			BETWE		392,00
	OM:	0			0	TO	: B	H 4 ONDI	K HUIS	OND	ER HUIS	RO	KEHO	LES [km	ıj	



& TIME:	T STARTI 2 COMPLE 2 YIELD [I/s] 5,53 5,55 5,55	TED 021/10/2 TED 021/11/0 TIME [min] 1 2 3 5 7 10 15	28 07:00 23 07:00 RECOVERY [m] 58,66 54,18 49,36 44,52 36,76	OE WATI	STANT DISC SERVATION ER LEVEL [mbcl]: SING HEIGHT [m]: G DIAMETER [m]: DISTANCE [m]: DRAWDOWN [m]	N/A N/A N/A N/A	OB WATE CAS CASING	SERVATION R LEVEL [mbcl]: ING HEIGHT [m]: DIAMETER [m]: DISTANCE [m]:	HOLE 2 N/A N/A N/A	WATE	SERVATION ER LEVEL [mbcl]: SING HEIGHT [m]: G DIAMETER [m]:	N/A N/A
TEST & TIME: & TIME: & TIME: AWDOWN [m] 8,32 12,26 14,08 17,44 20,02 23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	T STARTI 2 COMPLE 2 YIELD [I/s] 5,53 5,55 5,55	TED 021/10/2 TED 021/11/0 TIME [min] 1 2 3 5 7 10 15	28 07:00 23 07:00 RECOVERY [m] 58,66 54,18 49,36 44,52 36,76	CASIN TIME: [min] 1 2 3	ER LEVEL [mbcl]: SING HEIGHT [m]: G DIAMETER [m]: DISTANCE [m]: DRAWDOWN	N/A N/A N/A N/A RECOVERY	WATE CAS CASING	R LEVEL [mbcl]: ING HEIGHT [m]: DIAMETER [m]: DISTANCE [m]:	N/A N/A N/A	WATE	ER LEVEL [mbcl]: SING HEIGHT [m]:	N/A N/A
& TIME: TEST & TIME: AWDOWN [m] 8,32 12,26 14,08 17,44 20,02 23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	2/COMPLE 2/YIELD [I/s] 5,53 5,55	021/10/2 TED 021/11/0 TIME [min] 1 2 3 5 7 10 15	03 07:00 RECOVERY [m] 58,66 54,18 49,36 44,52 36,76	CASIN TIME: [min] 1 2 3	SING HEIGHT [m]: G DIAMETER [m]: DISTANCE [m]: DRAWDOWN	N/A N/A N/A RECOVERY	CASING	ING HEIGHT [m]: DIAMETER [m]: DISTANCE [m]:	N/A N/A	CAS	SING HEIGHT [m]:	N/A
TEST & TIME: CAWDOWN [m] 8,32 12,26 14,08 17,44 20,02 23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	2: YIELD [I/s] 5,53 5,55	TED 021/11/0 TIME [min] 1 2 3 5 7 10 15	03 07:00 RECOVERY [m] 58,66 54,18 49,36 44,52 36,76	CASIN TIME: [min] 1 2 3	G DIAMETER [m]: DISTANCE [m]:	N/A N/A RECOVERY	CASING	DISTANCE [m]:	N/A	-		
8 TIME: CAWDOWN [m] 8,32 12,26 14,08 17,44 20,02 23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	2 YIELD [l/s] 5,53 5,55	021/11/0 TIME [min] 1 2 3 5 7 10	RECOVERY [m] 58,66 54,18 49,36 44,52 36,76	TIME: [min] 1 2 3	DISTANCE [m]: DRAWDOWN	N/A RECOVERY	TIME:	DISTANCE [m]:		0710111	O Dirane i Erc [].	11//
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8,32 12,26 14,08 17,44 20,02 23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	5,53 5,55 5,55	1 2 3 5 7 10	58,66 54,18 49,36 44,52 36,76	1 2 3	[m]	[m]	Land of	DRAWDOWN	RECOVERY	TIME:		RECOVER
12,26 14,08 17,44 20,02 23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	5,55	2 3 5 7 10 15	54,18 49,36 44,52 36,76	3			[min]	[m]	[m]	[min]	[m]	[m]
14,08 17,44 20,02 23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	5,55	3 5 7 10 15	49,36 44,52 36,76	3			1			1		
17,44 20,02 23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	5,55	5 7 10 15	44,52 36,76				2			2	 	
20,02 23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	5,55	7 10 15	36,76	5			3			3		-
23,52 28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	5,55	10 15		_			5			5		-
28,02 29,60 31,50 32,86 34,78 36,70 38,35 39,45	5,55	15		7			7			7		-
29,60 31,50 32,86 34,78 36,70 38,35 39,45			30,41	10			10			10		-
31,50 32,86 34,78 36,70 38,35 39,45			28,32	15 20			15 20			15 20		
32,86 34,78 36,70 38,35 39,45		30	27,86 27,38	30			30			30		
34,78 36,70 38,35 39,45	E E 4	40	26,88	40			40			40		-
36,70 38,35 39,45		60	26,02	60			60			60		
38,35 39,45	5,54	90	24,30	90			90			90		1
39,45	5,53	120	23,78	120			120			120		
	-,	150	23,04	150			150			150		
10,00	5,56	180	22,62	180			180			180		
41,47		210	21,43	210			210			210		
42,30	5,54	240	20,74	240			240			240		
43,45		300	19,06	300			300			300		
44,77	5,55	360	17,54	360			360			360		
45,68		420	17,28	420			420			420		
47,02	5,54	480	16,92	480			480			480		
47,98		540	16,78	540			540			540	<u> </u>	
48,77	5,52	600	16,64	600			600			600	ļ	
50,21		720	16,11	720			720			720		
51,80	5,56	840	15,52	840			840			840		-
52,55		960	14,74	960			960			960		-
53,68	5,53	1080	13,98	1080			1080			1080		-
54,08		1200	13,49	1200			1200			1200		-
54,80	5,55	1320 1440	12,96 12,74	1320 1440			1320 1440			1320 1440		
55,05 55,22	5,55	1560	12,74	1560			1560			1560		+
55,34	3,33	1680	11,84	1680			1680			1680		
55,72	5.55	1800	11,42	1800			1800			1800		
56,14	0,00	1920	11,21	1920			1920			1920		
56,42	5,54	2040	10,80	2040			2040			2040		
57,04		2160	10,38	2160			2160			2160		
57,52		2280	10,17	2280			2280			2280		
58,16	5,52	2400	9,86	2400			2400			2400		
58,92		2520	9,68	2520			2520			2520		
59,54		2640	9,52	2640			2640			2640		
60,02	5,56	2760	9,38	2760			2760			2760	ļ	
60,28		2880	9,13	2880			2880			2880	<u> </u>	-
60,50		3000	8,89	3000			3000			3000		-
60,64	5,54	3120	8,74	3120			3120			3120		1
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61,26	5,53	3360	8,49	3360			3360			3360		1
61,48	5 5 5	3480	8,29	3480			3480			3480		-
	3,33			1						1		+
	5 57											1
62 40	5,51		·	1						1		<u> </u>
62,40 62.81	5.55			1						1		
62,81	3,30		7,18	4200						1		<u> </u>
62,81 63,04	5,53	4320	6,94	4320			4320			4320		
62,81 63,04 63,38			4320		RECOVERY:	4320	OBS 1:	0	OBS 2:	0	OBS 3:	0
62,81 63,04 63,38 63,74					RECOVERY:	6,94	OBS 1:	0,00	OBS 2:	0,00	OBS 3:	
62,81 63,04 63,38 63,74 ATION TOTA					RECOVERY:	89,11	OBS 1:	0,00	OBS 2:	0,00	OBS 3:	
62,81 63,04 63,38 63,74 ATION TOTA		CDT:	5,54		COMMENTS:							
6	2,81 3,04 3,38 3,74 ON TOTA // RECOV	2,02 2,40 5,57 2,81 3,04 5,55 3,38 3,74 5,53 5,57 7,87 7,	2,02 3720 2,40 5,57 3840 2,81 3960 3,04 5,55 4080 3,38 4200 3,74 5,53 4320 ON TOTALS [min] CDT: // RECOVERY [m] CDT: // RECOVERY [%] CDT: ERAGE YIELD [/s] CDT:	2,02 3720 7,86 2,40 5,57 3840 7,70 2,81 3960 7,59 3,04 5,55 4080 7,38 3,38 4200 7,18 3,74 5,53 4320 6,94 ON TOTALS [min] CDT: 4320 I/ RECOVERY [m] CDT: 63,74 I/ RECOVERY [%] CDT: 80,72 ERAGE YIELD [l/s] CDT: 5,54	2,02	2,02 3720 7,86 3720 2,40 5,57 3840 7,70 3840 2,81 3960 7,59 3960 3,04 5,55 4080 7,38 4080 3,38 4200 7,18 4200 3,74 5,53 4320 6,94 4320 ON TOTALS [min] CDT: 4320 RECOVERY: // RECOVERY [m] CDT: 63,74 RECOVERY: // RECOVERY [%] CDT: 80,72 RECOVERY: ERAGE YIELD [I/s] CDT: 5,54 COMMENTS:	2,02 3720 7,86 3720 2,40 5,57 3840 7,70 3840 2,81 3960 7,59 3960 3,04 5,55 4080 7,38 4080 3,38 4200 7,18 4200 3,74 5,53 4320 6,94 4320 ON TOTALS [min] CDT: 4320 RECOVERY: 4320 RECOVERY: 6,94 7,00 RECOVERY: 6,94 RECOVERY: 6,94 RECOVERY: 6,94 RECOVERY: 6,94 RECOVERY: 89,11 RECOVERY: 89,11 CDT: 5,54 COMMENTS:	2,02	2,02	2,02 3720 7,86 3720 3720 3840 3720 3720 2,40 5,57 3840 7,70 3840 3840 3840 3840 3840 3840 3840 384	2,02	2,02



	Summary		Wisteria 2 - Magalies Farm BH2											
Applicable	Method	Sustainable yield (I/s)	Std. Dev	Early ⁻	T (m²/d)	Late T (m²/d)	S	AD used					
•	Basic FC	4.01	2.01		16	8.1		2.20E-03	70.5	4.014				
	Advanced FC													
	FC inflection point													
v	Cooper-Jacob	5.89	3.81			36.1	1	4.08E-10	70.5	5,891				
	FC Non-Linear													
V	Barker	5.64	4.05	K _f =	4		S _s =	1.00E-07	70.5	5.637				
	Average Q sust (I/s)	5.18	1.02	b =	0.10	Fractal dimension n	ı =	2.45						

Recommended abstraction r	ate (L/s)	5.81	20916	l/hr	For 24 hrs per day
Hours per day of pumping (L/s)	12	8.22	29592	l/hr	12 hrs per day
Hours per day of pumping (L/s)	10	9.00	32400	l/hr	10 hrs per day
Hours per day of pumping (L/s)	8	10.07	36252	l/hr	8 hrs per day

Amount of water allowed to be abstracted per month	15059.52	m ³
Borehole could satisfy the basic human need of	20079	persons
Is the water suitable for domestic use (Yes/No)	_	

Recommended pump depth below surface (m)	120	
Total Casing length	144	
Blow yield (I/s)	-	
Expected dynamic water level over 24hr pump	80	mbcl
Critical depth that water level must not exceeded	100	mbcl
Depth of BH	144	mbcl
Static Water Level	31.44	mbcl

metres below casing level



9 Schubert Road Walmer Heights Port-Elizabeth 6070 South Africa

T +27 (0) 82 099 2366 E divan@dhsgroundwater.co.za W https://dhsgroundwater.co.za

Divan Stroebel (Pr.Sci.Nat, MGSSA) Hydrogeologist - Director DHS Groundwater Consulting Services 15/10/2021

Management recommendations

The aquifer consists of a good fracture network with radial flow present. Transmissivity is in the order of 8.1 to 36.1 m2/day.

An available drawdown of 100 mbcl is recommended.

As a rule of thumb, 60% of the total available drawdown (depth between main water strike and static water level) can be utilised without jeopardizing aquifer sustainability.

A dynamic water level of 80 mbcl is anticipated over a 24hr pump schedule at a volume of 5.81 l/s.

The water level should not exceed 170 mbcl, which is referred to as the critical water level.

Consistent drawdown below the critical water level will have a negative impact on the aquifer sustainability and yield.

It is therefore HIGHLY recommended to monitor the water level closely during pumping, to prevent drawdown in excess of 100 mbcl.

A conduit should be installed alongside the pump to allow for the measurement of the water level.

A SABS APPROVED FLOW METER MUST BE INSTALLED AT THE IMMEDIATE PUMP OUTLET AT THE BOREHOLE TO ENSURE THE RECOMMENDED PUMP VOLUMES ARE NOT EXCEEDED.

PLEASE NOTE: Borehole is in close proximity to neighbouring boreholes. It is therefore of utmost importance to monitor water levels during abstraction within all boreholes.



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Borehole testing and associated projects

CC Registration nr: 2005/137492/23 18 Highfield Road, EAST LONDON, 5205 Cell: +27 (0)71 031 5086 Fax: +27 (0)86 517 9242

		201011010	testing and associated proje	
		В	OREHOLE TEST RECORD	
Borehole Number:	BH 3 LOERIE P	IVOT	Province:	EASTERN CAPE
Alternative Number:			District:	LOERIE
Coordinates: Latitude [°S]	33,903260		Town/Village/Farm:	LOERIE
Longitude [°E]			Rig Type & number:	
Date & Time Test Started:	2021/10/06 00	0:00	Operator:	
Date & Time Test Ended:	2021/10/11 00	0:00	Supervisor:	HERMAN
Consultant:				
CONSULTANT - DATA PR	OVIDED / INST	RUCTIONS:		EXISTING INSTALLATION:
	e depth [mbgl]:		Diesel/Electric/Wind/Hand	ELECTRIC
	Blow Yield [I/s]:		Pump Make & Serial no:	SUBMERSIBLE
	epth(s) [mbgl]:		Intallation Depth (m)	107 M
	n depth [mbgl]:		Type & Condition - Pump:	GOOD WORKING
	s [l/s] - Step 1:			RAKSHA 80 MM
	Step 2:		- Pump House	N/A
	Step 3:		-	FIELD MEASUREMENTS:
	Step 4:		Depth Before Test [mbcl]:	144,00
	Step 5:		Depth after Test [mbcl]:	144,00
	Step 6:		Water Level before Test [mbcl]:	31,44
Step	Duration [min]:		Water Level after Test [mbcl]:	33,52
Step Recovery	Duration [Hrs]:		Casing Depth [mbcl]:	PVC
Cons	tant Yield [I/s]:		Casing Height [magl]:	0,19
Constant	Duration [Hrs]:		Casing Diameter [mm]:	165,00
Recovery Duration [Hrs] /	Drawdown %:			TEST PUMP INSTALLATION DETAILS:
Lenghth of Layfla	t Required [m]:		Pump Used:	GW 9002
Frequency of pH and EC	Measurements:		Depth Installed [mbcl]:	130,00
SAMPLE IN	STRUCTIONS:	II.	Datum Level above Casing [m]:	0,47
			Length of Layflat [m]:	300,00
			GENERAL ACTIONS:	
Supplied new steel of	over [Yes/No]:	NO	Slug Test [Yes/No]:	N/A
· · Velded existing steel cover				p [Yes/No]: YES LEFT IT WORKING
	rking [Yes/No]:		If not, where was it stored?	N/A
Site Cleaning and Finis			Maintenance work [Hrs]:	-
Data Reporting and Recor			Maintenance Travel [km]:	-
Digital Photo Ta			List of parts replaced/repaired:	N/A
RETREAT	FROM SITE		Date &Time Sampled:	NO SAMPLE TAKEN
It is hereby acknowledged that existing equipment is in an ac			COM	IMENTS BY ONSITE CREW
NAME:				
DESIGNATION:				
SIGNATURE:				
DATE:			***************************************	
DAIE.	1			



BOREHO	LE NO: BH 3	LOERIE P	VOT W	VATER LEVE			31,91			TH [mbgl]:	31,25	AVA	ILABLE	DRAWE	OOWN [m]	98,56									
DIC	CITA DOD DAG	TD 1	RPM			STEPPED DISCHAR			EST & F	RECOVER		DICCLIADO	3 D 4 /	7D 0	RPM										
	CHARGE RAT		1/10/06 1	5.00		DISCHARI TE & TIME	GE RA		1/10/06 16:	00		DISCHARGI ATE & TIME	E RAI	.E 3	-	/06 17:00									
TIME	DRAWDOWN	YIELD	TIME	RECOVER			/DOWN	YIELD	TIME	RECOVE			ww	YIELD	TIME	RECOVERY									
(min)	(m)	(I/s)	(min)	(m)	(min		m)	(I/s)	(min)	(m)	(mir			(I/s)	(min)	(m)									
1	6,64		1		1	11	,54		1		1	30, 2	2		1										
2	7,42		2		2		2,62		2		2	34,6	_		2										
3	7,80	2,33	3		3		3,48	4,74	3		3	39,5	_	10.01	3										
5 7	8,02		5 7		5 7		.,52 .,93		5 7		5 7	44,10		10,24	5 7										
10	8,11 8,26	2,35	10		10		5,38		10		10	50,3			10										
15	8,34		15		15		5,88	5,02	15		15	52,6		10,24	15										
20	8,82		20		20	17	7,56		20		20	54, 2	0		20										
30	9,24	2,33	30		30), 28		30		30	54,9			30										
40	9,56	0.04	40		40		3,12	5,02	40		40	55,4	_	10,24	40										
50 60	9,95	2,34	50 60		50 60		3,86 1,74		50 60		50 60	56, 10 57, 0			50 60										
00	10,12		70		- 00	ZA	t, /4		70		00	37,0	-		70										
			80						80						80										
			90						90						90										
			100						100						100										
			110	-	\perp				110		\perp		_		110										
			120 150	-	-	-			120 150				-		120 150										
Δν	erage Yield (I/s):	2,34	180			Average Yie	eld (l/s).	5,01	180			Average Yield	(l/s):	10,24	180										
AV	Drawdown (%):		210				wn (%):		210			Drawdown	• •	57,85	210										
DIS	CHARGE RAT		RPM		1	DISCHAR			RPM			DISCHARGI	• • •	E 6	RPM										
DATE	& TIME	202	1/10/06 1	8:00	DAT	TE & TIME		202	1/10/06 18:	00	D					DATE & TIME		DATE & TIME						2021/10	/06 18:00
TIME	DRAWDOWN	YIELD	TIME	RECOVER	Y TIME	DRAW	VDOWN	YIELD	TIME	RECOVE	RY TIM	E DRAWDO	OWN	YIELD	TIME	RECOVERY									
(min)	(m)	(I/s)	(min)	(m)	(min) (1	m)	(I/s)	(min)	(m)	(mir	n) (m)		(l/s)	(min)	(m)									
1	61,24		1		1				1		1				1	50,28									
3	64,42 65,70	12.52	3		3				3		2				3	42, 16 36, 40									
5	66,62	12,02	5		5				5		5				5	30,62									
7	70,34	15,06	7		7				7		7				7	26,32									
10	72,40		10		10				10		10				10	20, 14									
15	74,56		15		15				15		15				15	17,36									
20	75,48	15,05	20		20				20		20				20	14,26									
30 40	76,6 78,36		30 40		30 40				30 40		30 40		-		30 40	10,88 9,64									
50	81,24	15,06	50		50				50		50				50	8,72									
60	84,06	,	60		60				60		60				60	7,52									
	,		70						70						70	6,66									
			80						80						80	5,92									
			90						90						90	5,48									
			100 110		+				100 110						100 110	4,86 4,34									
			120		+				120		-+				120	3,84									
			150						150						150	3,40									
			180						180						180	2,64									
			210						210						210	2,41									
_		41.55	240			A	.14.01.1		240			A	nı->	0.00	240	2,21									
Av	erage Yield (I/s): Drawdown (%):		300 360	-		Average Yie	eld (l/s): own (%):	-	300 360			Average Yield Drawdown	• •	0,00	300 360	2,08 1,86									
DATUM I	EVEL ABOVE GR			<u>. </u>		DIAWOO	vvii (%):	1		D PUMPED ?	? NO	awdown	(/0).		JUUU	1,00									
	VATER LEVEL AF				[mbdl]:	31,91				WATER CLE		i													
	DURATION	DRAWDO	I/N	AVERAGE		STEP: RECOVERY	PED D		WN SUM		JOWN!	AVERAGE			RECOVE	DV									
STEP		m]	[%]	YIELD [I/s]	[min]	[m]	[%]	STEP	[min]	[m]	[%]	YIELD [I/s]	[min]		[m]	[%]									
1			10,27	2,34				5		0,00		0,00													
2			25,10	5,01				6		0,00		0,00													
3		-	57,85	10,24				7																	
4 DATE &	60 84 TIME END:		85,29 2021/10/0	14,96				8 TOTAL:	240,00	84,06	85,29		0		0,00	0,00									
COMME		4	LUZ 1/1U/U	00.EI 00				IUIAL:	240,00	04,00	03,29		U		0,00	0,00									
J - 111111L																									
						HMENT						ESTAB				2021/10/06									
	MOVE	BOREHO	LE		AGE	MOV		BOREH			LAGE			BETWE		392,00									
FR	OM:	0			0	TO:	: BH	13 LOER	E PIVOT	L LC	DERIE	BOF	KEHOL	ES [km]	,···									



	HOLE NO:		O LOLI	RIE PIVOT	CON	STANT DISC	EVEL [mbdl]: HARGE TE		31,91 RECOVERY		WATEN	R LEVEL [mbgl]:	31,25
	DISCHARGE	BORE	HOLE	2	_	SERVATION			SERVATION	HOLE 2	OE	SERVATION	HOLE 3
		STARTI		-	+	ER LEVEL [mbcl]:	N/A		R LEVEL [mbcl]:	N/A	1	ER LEVEL [mbcl]:	N/A
D.	ATE & TIME:			07 07:30	-1	SING HEIGHT [m]:	N/A	-	SING HEIGHT [m]:	N/A	-1	SING HEIGHT [m]:	N/A
		COMPLE	TED		4	G DIAMETER [m]:	N/A	-	G DIAMETER [m]:	N/A	-1	G DIAMETER [m]:	N/A
D.	ATE & TIME:	2	021/10/	13 07:30	1	DISTANCE [m]:	N/A		DISTANCE [m]:	N/A	1	DISTANCE [m]:	N/A
ГІМЕ	DRAWDOWN	YIELD	TIME	RECOVERY	TIME:	DRAWDOWN	RECOVERY	TIME:	DRAWDOWN	RECOVERY	TIME:	DRAWDOWN	RECOVER
[min]	[m]	[l/s]	[min]	[m]	[min]	[m]	[m]	[min]	[m]	[m]	[min]	[m]	[m]
1	8,21		1	48,95	1			1			1		
2	12,38		2	46,72	2			2			2		
3	14,93	0.00	3	42,33	3			3			3		
5	17,03	9,03	5	35,64	5			5			5		
7 10	20,52 24,87		7 10	30,54	7 10			7 10			7 10		
15	31,20	9,05	15	25,96 22,80	15			15			15		
20	36,80	9,03	20	19,65	20			20			20		
30	38,79	9,02	30	16,52	30			30			30		
40	39,70	3,02	40	14,33	40			40			40		
60	40,30	9,05	60	12,36	60			60			60		
90	40,53	-,••	90	10,96	90			90			90		
120	40,79	9,02	120	7,84	120			120			120		
150	41,06		150	7,78	150			150			150		
180	41,38	9,04	180	7,76	180			180			180		
210	41,69		210	7,62	210			210			210		
240	42,03	9,07	240	7,56	240			240			240		
300	42,29		300	7,50	300			300			300		
360	42,40	9,07	360	7,45	360			360			360		
420	42,78		420	7,39	420			420			420		
480	42,98		480	7,28	480			480			480		
540	43,18	9,06	540	7,24	540			540			540		
600	43,36		600	7,20	600			600			600		
720	43,58	9,05	720	7,19	720			720			720		
840	43,74		840	7,18	840			840			840		
960	44,02		960	7,15	960			960			960		
1080	44,20	9,08	1080	7,12	1080			1080			1080		
1200	44,39		1200	7,08	1200			1200			1200		
1320 1440	44,62 44,94	9,06	1320 1440	7,05 6,84	1320 1440			1320 1440			1320 1440		
1560	45,26	9,00	1560	6,62	1560			1560			1560		
1680	45,54		1680	6,44	1680			1680			1680		
1800	45,96	9.04	1800	6,24	1800			1800			1800		
1920	46,42	3,04	1920	6,03	1920			1920			1920		
2040	46,86	9,07	2040	5,80	2040			2040			2040		
2160	47,38	.,	2160	5,65	2160			2160			2160		
2280	47,80	9,06	2280	5,36	2280			2280			2280		
2400	48,12		2400	4,82	2400			2400			2400		
2520	48,44	9,08	2520	4,34	2520			2520			2520		
2640	48,80		2640	4,12	2640			2640			2640		
2760	49,06		2760	3,89	2760			2760			2760		
2880	49,42	9,09	2880	3,65	2880			2880			2880		
3000	49,68		3000		3000			3000			3000		
3120	49,93	9,10	3120		3120			3120			3120		
3240	50,15		3240		3240			3240			3240		
3360	50,43	9,05	3360		3360			3360			3360		
3480	50,72	_	3480		3480			3480			3480		
3600	50,94	9,04	3600		3600			3600			3600		
3720	51,22		3720		3720			3720			3720		
3840	51,40	0.00	3840		3840			3840			3840		
3960	51,64	9,06	3960		3960			3960			3960		
4080	51,82	0.05	4080		4080			4080			4080		
4200	52,06 52.28	9,05	4200		4200			4200			4200		
4320	52,28	 C !:1	4320	4000	4320	DECOVERY	4220	4320 OBS 1:	^	ODE 1:	4320	0000	
	URATION TOTA			4320		RECOVERY:	4320	OBS 1:		OBS 2:	0,00	OBS 3:	
	/DOWN / RECOV /DOWN / RECOV			52,28 53,04		RECOVERY:	3,65 93,02	OBS 1: OBS 1:	0,00	OBS 2: OBS 2:	0,00	OBS 3:	0,00
~:\AV	AVERAGE YI			9,06		COMMENTS:	JJ,UZ	1: DGG	0,00	J J J J Z.	0,00	J J J J J J	0,00
				0,00		JOHNHLATIO.							



	Summary			Wis	teria 2 -	Spoorbrug	BH1			
Applicable	Method	Sustainable yield (l/s)	Std. Dev	Early ⁻	Γ (m²/d)	Late T (m²/d)	S	AD used	Ī
~	Basic FC	9.57	4.73	2	20	13.	7	2.20E-03	101.2	9.5/1583
	Advanced FC									
	FC inflection point									
✓	Cooper-Jacob	10.17	6.59			22.	6	1.63E-03	101.2	10.17491
	FC Non-Linear									
~	Barker	11.74	7.27	K _f =	52		S _s =	1.00E-07	101.2	11.79508
	Average Q_sust (I/s)	10.49	1.12	b =	0.10	Fractal dimension i	n =	2.16		

Recommended abstraction r	ate (L/s)	10.49	37764	l/hr	For 24 hrs per day
Hours per day of pumping (L/s)	12	14.84	53424	l/hr	12 hrs per day
Hours per day of pumping (L/s)	10	16.25	58500	l/hr	10 hrs per day
Hours per day of pumping (L/s)	8	18.17	65412	l/hr	8 hrs per day

Amount of water allowed to be abstracted per month	27190.08	m ³
Borehole could satisfy the basic human need of	36253	persons
Is the water suitable for domestic use (Yes/No)	-	

Recommended pump depth below surface (m) 120

Total Casing length 248.40

Blow yield (l/s)
Expected dynamic water level over 24hr pump 60 mbcl

Critical depth that water level must not exceeded 105 mbcl

Depth of BH 248.40 mbcl

Static Water Level 4.10 mbcl

metres below casing level



9 Schubert Road Walmer Heights Port-Elizabeth 6070 South Africa

T +27 (0) 82 099 2366 E divan@dhsgroundwater.co.za W https://dhsgroundwater.co.za

Divan Stroebel (Pr.Sci.Nat, MGSSA)

Hydrogeologist - Director

DHS Groundwater Consulting Services
15/10/2021

Management recommendations

The aquifer consists of a good fracture network with radial flow present. Transmissivity is in the order of 13.7 to 22.6 m2/day.

An available drawdown of 105 mbcl is recommended.

As a rule of thumb, 60% of the total available drawdown (depth between main water strike and static water level) can be utilised without jeopardizing aquifer sustainability.

A dynamic water level of 60 mbcl is anticipated over a 24hr pump schedule at a volume of 10.49 l/s.

The water level should not exceed 105 mbcl, which is referred to as the critical water level.

Consistent drawdown below the critical water level will have a negative impact on the aquifer sustainability and yield.

It is therefore HIGHLY recommended to monitor the water level closely during pumping, to prevent drawdown in excess of 105 mbcl.

A conduit should be installed alongside the pump to allow for the measurement of the water level.

A SABS APPROVED FLOW METER MUST BE INSTALLED AT THE IMMEDIATE PUMP OUTLET AT THE BOREHOLE TO ENSURE THE RECOMMENDED PUMP VOLUMES ARE NOT EXCEEDED.

PLEASE NOTE: Borehole is in close proximity to neighbouring boreholes. It is therefore of utmost importance to monitor water levels during abstraction within all boreholes.



Scenic route 565 t/a Welltek Services Vat nr: 45902 54720 Email: welltekservices@gmail.com



CC Registration nr: 2005/137492/23 18 Highfield Road, EAST LONDON, 5205 Cell: +27 (0)71 031 5086 Fax: +27 (0)86 517 9242

		Borehole	testing and associated proje	ects
		В	OREHOLE TEST RECORD	
Borehole Number:	BH 1		Province:	EASTERN CAPE
Alternative Number:			District:	LOERIE
Coordinates: Latitude [°S]	33,912250		Town/Village/Farm:	LOERIE
Longitude [°E]	24,953550		Rig Type & number:	PERKINS
Date & Time Test Started:	2021/08/20 00	0:00	Operator:	WASHINGTON
Date & Time Test Ended:	2021/08/27 00	0:00	Supervisor:	HERMAN
Consultant:				
CONSULTANT - DATA PR	OVIDED / INST	RUCTIONS:		EXISTING INSTALLATION:
Borehole	e depth [mbgl]:		Diesel/Electric/Wind/Hand	N/A
В	low Yield [l/s]:		Pump Make & Serial no:	N/A
Water Strike De	epth(s) [mbgl]:		Intallation Depth (m)	N/A
Installation	n depth [mbgl]:		Type & Condition - Pump:	N/A
Estimated Step	s [l/s] - Step 1:		- Column:	N/A
	Step 2:		- Pump House	N/A
	Step 3:			FIELD MEASUREMENTS:
	Step 4:		Depth Before Test [mbcl]:	248,40
	Step 5:		Depth after Test [mbcl]:	248,40
	Step 6:		Water Level before Test [mbcl]:	4,10
Step I	Duration [min]:		Water Level after Test [mbcl]:	8,89
Step Recovery	Duration [Hrs]:		Casing Depth [mbcl]:	PVC
Const	tant Yield [l/s]:		Casing Height [magl]:	0,46
Constant	Duration [Hrs]:		Casing Diameter [mm]:	186,00
Recovery Duration [Hrs] /	Drawdown %:			TEST PUMP INSTALLATION DETAILS:
Lenghth of Layfla	t Required [m]:		Pump Used:	GW 9002
Frequency of pH and EC	Measurements:		Depth Installed [mbcl]:	120,00
SAMPLE IN	STRUCTIONS:		Datum Level above Casing [m]:	0,34
			Length of Layflat [m]:	100,00
			GENERAL ACTIONS:	
Supplied new steel of	over [Yes/No]:	NO	Slug Test [Yes/No]:	N/A
Velded existing steel cover	back on [Y/N]:	NO	Re-install existing pum	p [Yes/No]: N/A
Borehole Mai	rking [Yes/No]:	NO	If not, where was it stored?	N/A
Site Cleaning and Finis	shing [Yes/No]:	YES	Maintenance work [Hrs]:	N/A
Data Reporting and Recor	ding [Yes/No]:	YES	Maintenance Travel [km]:	N/A
Digital Photo Ta	aken? [Yes/No]	NO	List of parts replaced/repaired:	N/A
RETREAT	FROM SITE		Date &Time Sampled:	NO SAMPLE TAKEN
It is hereby acknowledged tha	at upon leaving th	e site, all	COM	MENTS BY ONSITE CREW
existing equipment is in an ac	ceptable conditior	1.		
NAME:				
DESIGNATION:				
SIGNATURE:				
DATE:				



REHOLE	E NO:	BH 1	W	ATER LEVEL [4,44			TH [mbgl]:	3,64	ı	AVAILAB	LE DRAW	OOWN [m]	: 115,90
DIOC	WILL DOD D. I	T 1	DDM							RECOVER	Y	DIGGI	LA DOD D		DDM	
DISC BATE &	CHARGE RAT		RPM 1/08/21 1	1.15	_	SCHARG & TIME	E RA		RPM 1/08/21 12:	45		DISCH ATE & TI	IARGE RA	ATE 3	RPM	124 42:45
	DRAWDOWN	YIELD	TIME	RECOVERY	TIME	DRAW	DOWN	YIELD	TIME	RECOVE			RAWDOWN	YIELD	TIME	21 13:15 RECOVERY
n)	(m)	(l/s)	(min)	(m)	(min)	(m		(I/s)	(min)	(m)	(mi		(m)	(l/s)	(min)	(m)
	1,62	, ,	1	, ,	1	18,	90	, ,	1	, ,	1		29,08		1	, ,
	2,84		2		2	19,			2		2		29,80		2	
	4,56	0.50	3		3	19,		9,17	3		3		30,21	15, 12	3	
	6,94 10,22	6,53	5 7		5 7	19, 20,		9.18	5 7		5 7		30,94		5 7	
	12,62	5,06	10		10	20,		3, 10	10		10		32,08	15,12	10	
	13, 19	-,	15		15	20,			15		15		32,72		15	
	14,69		20		20	21,	09	9, 18	20		20		33, 24		20	
	15, 12	5,08	30		30	21,			30		30		34,06	15, 11	30	
	15,62		40 50		40 50	22,		9, 18	40 50		40 50		34,80 35,40	15, 13	40 50	
	16,06 16,54	5,07	60		60	23,			60		60		36,09	15, 13	60	
	10,01	0,01	70		100	20,	10		70				00,00		70	
			80						80						80	
	<u> </u>		90						90						90	
\perp			100		-	1			100						100	
			110 120		-	+			110 120						110 120	
-			150			+			150						150	+
Avei	rage Yield (I/s):	5,14	180		Ave	erage Yiel	ld (I/s):	9,18	180			Average	Yield (I/s):	15,12	180	<u> </u>
	Drawdown (%):	14,27	210			Drawdov	wn (%):	20,24	210			Drav	wdown (%):	31,14	210	
DISC	CHARGE RAT	Έ 4	RPM		DIS	CHARG	E RA	TE 5	RPM			DISCH	IARGE RA	ATE 6	RPM	
DATE &	TIME	202	1/08/21 1	4:15	DATE	& TIME		202	1/08/21 14:	15	D	ATE & TI	IME		2021/08/	21 14:15
	DRAWDOWN	YIELD	TIME	RECOVERY	TIME	DRAWI		YIELD	TIME	RECOVE			RAWDOWN	YIELD	TIME	RECOVERY
n)	(m)	(I/s)	(min)	(m)	(min)	(m	1)	(I/s)	(min)	(m)	(mi	n)	(m)	(l/s)	(min)	(m)
+	37,76 38,64		2		2				2		1 2				2	26,94 21,84
	39,90	20.62	3		3				3		3				3	17,76
	40,67		5		5				5		5				5	17,64
	42,54		7		7				7		7				7	16,23
	43, 26	25,08	10		10				10		10				10	14,90
_	44,02 44,88		15 20		15 20				15 20		15 20				15 20	13,78 12,60
-	45,84	25,08	30		30				30		30				30	11,08
	46,64	20,00	40		40				40		40				40	10,68
	47,28	25,06	50		50				50		50				50	9,25
	47,7		60		60				60		60				60	8,57
_			70						70						70	7,97
			80 90						80 90						80 90	7,62 7,20
			100						100						100	6,86
			110			L			110						110	6,57
			120						120						120	6,29
			150						150						150	5,65
+			180 210			1			180 210						180 210	5,04
+			240			1			240			-			240	4,83 4,60
Avei	rage Yield (I/s):	24,93	300		Ave	erage Yiel	ld (I/s):	0,00	300			Average	Yield (I/s):	0,00	300	4,38
	Drawdown (%):	41,16	360			Drawdov	. ,		360				wdown (%):		360	4,07
	VEL ABOVE GR	<u> </u>								D PUMPED 1						
ATIC WA	ATER LEVEL AF	TER STEP	PED DISC	HARGE TEST [mbdl]:	4,44			WAS THE	WATER CLE	EAN? YES	S				
						STEPP	ED D	RAWDO	WN SUM	MARY						
TEP D	DURATION	DRAWDO		AVERAGE		OVERY		STEP	DURATION	DRAWE		AVER	-		RECOVE	1
		n]	[%]		min]	[m]	[%]		[min]	[m]	[%]	YIELD		in]	[m]	[%]
2			14,27 20,24	5,14 9,18				5 6		0,00		0,0				
3	60 36		20,24 31,14	15,12				7		0,00		0,0	•	+		+
4			41,16	24,93				8				1				<u> </u>
TE & T	IME END:	_	2021/08/2					TOTAL:	240,00	47,70	41,16		()	0,00	0,00
MMEN.	TS:															
				7300	A DI IOI	MENT						-	STADI ICI	IMENT D	TE.	2024/00/20
SITE N	MOVE	BOREHO) F	VILLA	ABLISHI GF	MENT	=	BOREH	IOI F	VII	LAGE		STABLISH DISTANCE			2021/08/20
FRO		0		0	·~-	TO:	-	BH								392,00
FRO	DM:	0		0		TO:		ВН	1	LC	DERIE		BOREHO	OLES [km	1	35



DUKE	HOLE NO:		BH		COM	WATER L STANT DISC	EVEL [mbdl]: HARGE TE		4,44 RECOVERY		vva i ER	R LEVEL [mbgl]:	3,64
	DISCHARGE	BORE	HOLE	· · · · · ·		SERVATION			RECOVERY SERVATION	HOLE 2	OF	SERVATION	HOLES
		STARTI		•	1	ER LEVEL [mbcl]:	N/A	1	R LEVEL [mbcl]:	N/A	1	ER LEVEL [mbcl]:	N/A
DA	ATE & TIME:			27 07:29	1	SING HEIGHT [m]:	N/A	-1	SING HEIGHT [m]:	N/A	-1	SING HEIGHT [m]:	N/A
	TEST	COMPLE	TED		CASIN	G DIAMETER [m]:	N/A	CASING	G DIAMETER [m]:	N/A	CASIN	G DIAMETER [m]:	N/A
DA	ATE & TIME:	2	021/09/0	02 07:29		DISTANCE [m]:	N/A		DISTANCE [m]:	N/A		DISTANCE [m]:	N/A
TIME	DRAWDOWN	YIELD		RECOVERY	TIME:	DRAWDOWN	RECOVERY	TIME:	DRAWDOWN	RECOVERY	TIME:	DRAWDOWN	RECOVER
[min]	[m]	[l/s]	[min]	[m]	[min]	[m]	[m]	[min]	[m]	[m]	[min]	[m]	[m]
1	7,84		2	52,32	1			1			2		
3	11,21 16,53	15,93	3	48,19 44,48	3			3			3		
5	19,97	13,33	5	39,49	5			5			5		
7	26,60		7	38,12	7			7			7		
10	27,74	16,13	10	35,71	10			10			10		
15	29,06		15	33,70	15			15			15		
20	31,05	16,14	20	32,55	20			20			20		
30	31,93		30	31,51	30			30			30		
40	33,22		40	30,56	40			40			40		
60	35,16	16,13	60	29,64	60			60			60		
90	37,16	4	90	27,81	90			90			90		
120	38,53	16,14	120	26,20	120			120			120		
150	39,70	16 10	150	24,50	150			150			150		
180 210	40,39 41,40	16,12	180 210	22,38 20,90	180 210			180 210			180 210		
240	41,40	16,13	240	20,90	240			240			240		
300	42,80	.0,10	300	18,50	300			300			300		
360	43,67	16,14	360	17,85	360			360			360		
420	44,36	Ĺ	420	17,48	420			420			420		
480	45,12	16,15	480	16,37	480			480			480		
540	46,36		540	15,24	540			540			540		
600	47,46	16,13	600	14,55	600			600			600		
720	48,21		720	13,95	720			720			720		
840	49,07	16,12	840	13,30	840			840			840		
960	49,75		960	12,95	960			960			960		
1080	50,28	16,14	1080	11,70	1080			1080			1080		
1200 1320	50,71	46.40	1200	11,12	1200			1200			1200		
1440	51,15 51,22	16,12	1320 1440	10,67 10,24	1320 1440			1320 1440			1320 1440		
1560	51,58	16,14	1560	9,47	1560			1560			1560		
1680	51,89	10,14	1680	8,97	1680			1680			1680		
1800	52,05	16,15	1800	8,55	1800			1800			1800		
1920	52,22	ĺ	1920	8,23	1920			1920			1920		
2040	52,43	16,13	2040	7,95	2040			2040			2040		
2160	52,54		2160	7,67	2160			2160			2160		
2280	52,71	16,15	2280	7,40	2280			2280			2280		
2400	52,94		2400	7,16	2400			2400			2400		
2520	53,07	16,14	2520	6,94	2520			2520			2520		
2640	53,21	16 44	2640	6,73	2640			2640			2640		
2760 2880	53,43 53,69	16,14	2760 2880	6,61 6,39	2760 2880			2760			2760		
3000	53,69 53,87	16,12	3000	6,39	3000			2880 3000			2880 3000		
3120	54,02	10,12	3120	6,02	3120			3120			3120		
3240	54,33	16,15	3240	5,82	3240			3240			3240		
3360	54,69		3360	5,62	3360			3360			3360		
3480	54,81	16,14	3480	5,39	3480			3480			3480		
3600	54,99		3600	5,03	3600			3600			3600		
3720	55,19	16,13	3720	4,87	3720			3720			3720		
3840	55,52		3840	4,66	3840			3840			3840		
3960	55,76	16,17	3960	4,41	3960			3960			3960		
4080	55,87	4	4080	4,23	4080			4080			4080		
4200	56,10	16,15	4200	4,08	4200			4200			4200		
4320	56,93	 C r= · ·	4320	3,89	4320	DECOVERY	4222	4320	^	0000	4320	0000	
	URATION TOTA			4320		RECOVERY:	4320	OBS 1:	0 00	OBS 2:	0	OBS 3:	0
	DOWN / RECOV			56,93 49,12		RECOVERY:	3,89 93,17	OBS 1: OBS 1:	0,00	OBS 2:	0,00	OBS 3: OBS 3:	0,00
- NAVV	AVERAGE YI			16,14		COMMENTS:	33,11	lono I:	0,00	J D J Z.	0,00	J J J J J J	0,00
	LIVIOL II	["3]	-P1:	. •, . •									



	Summary	Wisteria 2 - Spoorbrug BH 2											
Applicable	Method	Sustainable yield (l/s)	Std. Dev	Early ⁻	Γ (m²/d)	Late T (m²/d)	S	AD used				
▼	Basic FC	8.56	4.31		16	10.8	8	2.20E-03	113.2	8,5957			
	Advanced FC												
	FC inflection point												
▽	Cooper-Jacob	9.13	5.91			17.0	0	3.32E-03	113.2	9.12581			
	FC Non-Linear												
~	Barker	9.45	5.37	K _f =	164		S _s =	1.00E-07	113.2	9.45441			
	Average Q_sust (I/s)	9.05	0.45	b =	0.10	Fractal dimension r	1 =	2.00					

Recommended abstraction re	ate (L/s)	9.05	32580	l/hr	For 24 hrs per day
Hours per day of pumping (L/s)	12	12.80	46080	l/hr	12 hrs per day
Hours per day of pumping (L/s)	10	14.02	50472	l/hr	10 hrs per day
Hours per day of pumping (L/s)	8	15.68	56448	l/hr	8 hrs per day

Amount of water allowed to be abstracted per month	23457.6	m ³
Borehole could satisfy the basic human need of	31277	persons
Is the water suitable for domestic use (Yes/No)	-	

Recommended pump depth below surface (m) 135 Total Casing length 248 Blow yield (I/s) Expected dynamic water level over 24hr pump 75 mbcl Critical depth that water level must not exceeded 130 mbcl Depth of BH 248 mbcl Static Water Level **16.98** mbcl

metres below casing level



9 Schubert Road Walmer Heights Port-Elizabeth 6070 South Africa

T +27 (0) 82 099 2366 E divan@dhsgroundwater.co.za W https://dhsgroundwater.co.za

Divan Stroebel (Pr.Sci.Nat, MGSSA) Hydrogeologist - Director

DHS Groundwater Consulting Services 15/10/2021

Management recommendations

The aquifer consists of a good fracture network with radial flow present. Transmissivity is in the order of 10.8 to 17.0 m2/day.

An available drawdown of 130 mbcl is recommended.

As a rule of thumb, 60% of the total available drawdown (depth between main water strike and static water level) can be utilised without jeopardizing aquifer sustainability.

A dynamic water level of 75 mbcl is anticipated over a 24hr pump schedule at a volume of 9.05 l/s.

The water level should not exceed 130 mbcl, which is referred to as the critical water level.

Consistent drawdown below the critical water level will have a negative impact on the aguifer sustainability and yield.

It is therefore HIGHLY recommended to monitor the water level closely during pumping, to prevent drawdown in excess of 130 mbcl.

A conduit should be installed alongside the pump to allow for the measurement of the water level.

A SABS APPROVED FLOW METER MUST BE INSTALLED AT THE IMMEDIATE PUMP OUTLET AT THE BOREHOLE TO ENSURE THE RECOMMENDED PUMP VOLUMES ARE NOT EXCEEDED.

PLEASE NOTE: Borehole is in close proximity to neighbouring boreholes. It is therefore of utmost importance to monitor water levels during abstraction within all boreholes.



Scenic route 565 t/a Welltek Services Vat nr: 45902 54720 Email: welltekservices@gmail.com



Borehole testing and associated projects

CC Registration nr: 2005/137492/23 18 Highfield Road, EAST LONDON, 5205 Cell: +27 (0)71 031 5086 Fax: +27 (0)86 517 9242

		Dorentie	testing and associated proje	ects
		В	OREHOLE TEST RECORD	
Borehole Number:	BIG HOLE		Province:	EASTERN CAPE
Alternative Number:			District:	LOERIE
Coordinates: Latitude [°S]	33,908863		Town/Village/Farm:	LOERIE
Longitude [°E]	24,948775		Rig Type & number:	NISSAN
Date & Time Test Started:	2020/09/28 00	0:00	Operator:	JOE
Date & Time Test Ended:	2020/10/01 00	0:00	Supervisor:	HERMAN
Consultant:				
CONSULTANT - DATA PR	OVIDED / INST	RUCTIONS:		EXISTING INSTALLATION:
Borehole	e depth [mbgl]:		Diesel/Electric/Wind/Hand	N/A
В	low Yield [I/s]:		Pump Make & Serial no:	N/A
Water Strike D	epth(s) [mbgl]:		Intallation Depth (m)	N/A
Installation	n depth [mbgl]:		Type & Condition - Pump:	N/A
Estimated Step	s [l/s] - Step 1:		- Column:	N/A
	Step 2:		- Pump House	N/A
	Step 3:			FIELD MEASUREMENTS:
	Step 4:		Depth Before Test [mbcl]:	234,70
	Step 5:		Depth after Test [mbcl]:	234,70
	Step 6:		Water Level before Test [mbcl]:	14,46
Step	Duration [min]:		Water Level after Test [mbcl]:	14,46
Step Recovery	Duration [Hrs]:		Casing Depth [mbcl]:	PVC
Cons	tant Yield [I/s]:		Casing Height [magl]:	0,38
Constant	Duration [Hrs]:		Casing Diameter [mm]:	160,00
Recovery Duration [Hrs] /	Drawdown %:			TEST PUMP INSTALLATION DETAILS:
Lenghth of Layfla	t Required [m]:		Pump Used:	BP 40 M
Frequency of pH and EC	Measurements:		Depth Installed [mbcl]:	122,00
SAMPLE IN	STRUCTIONS:		Datum Level above Casing [m]:	0,20
			Length of Layflat [m]:	50,00
			GENERAL ACTIONS:	
Supplied new steel of	over [Yes/No]:	NO	Slug Test [Yes/No]:	N/A
Velded existing steel cover	back on [Y/N]:	NO	Re-install existing pump	[Yes/No]: N/A
Borehole Mai	rking [Yes/No]:	NO	If not, where was it stored?	N/A
Site Cleaning and Finis	shing [Yes/No]:	YES	Maintenance work [Hrs]:	N/A
Data Reporting and Recor	ding [Yes/No]:	YES	Maintenance Travel [km]:	N/A
Digital Photo Ta	aken? [Yes/No]	NO	List of parts replaced/repaired:	N/A
RETREAT	FROM SITE		Date &Time Sampled:	NO SAMPLE TAKEN
It is hereby acknowledged that existing equipment is in an ac			COM	IMENTS BY ONSITE CREW
NAME:				
DESIGNATION:				
SIGNATURE:				
DATE:				



BOREHO	LE NO:	BIG HOLE	v	VATER LEVEL [4,66		ATER DEP		14,08	AVA	AILABLE	DRAWI	DOWN [m]:	107,54
-			DD14							RECOVER					DDM	
	CHARGE RA		RPM			CHARG	E RA		RPM			DISCHARG	E RAT	Е 3	RPM	
	& TIME		20/09/28 1		DATE 8				0/09/28 14:			TE & TIME	01111	\//ELD	2020/09/2	
TIME (min)	DRAWDOWN (m)	YIELD (I/s)	TIME (min)	RECOVERY (m)	TIME (min)	DRAWD (m		YIELD (I/s)	TIME (min)	RECOVER (m)	RY TIME (min)			YIELD (I/s)	TIME (min)	RECOVERY (m)
1	2,82	(1/5)	1	(111)	1	14,2	,	(1/0)	1	(111)	1	26,0		(110)	1	()
2	3,89		2		2	14,			2		2	27,0			2	
3	4,62	2,18	3		3	15,	12	3,82	3		3	27,3	34	7,67	3	
5	5,55		5		5	16,8	85		5		5	29,8	35	8,02	5	
7	6,27		7		7	18,	29	4, 14	7		7	32, 3	37		7	
LO	7,25		10		10	19,			10		10	33,2			10	
L5	8,88		15		15	20,1			15		15	36,4			15	
20	9,89	2,17	20		20	21,0			20		20	37,7		8,02	20	
30	11,29	-	30		30	22,8		4,12	30		30	39,3			30	
10 50	12,35		40 50		40 50	23,8 24,8			40 50		40 50	40,9	_	8,02	40 50	
30 30	13,30 14,11		60		60	25,4			60		60	43,5		0,02	60	
	14,11		70		100	20,	+2		70		- 00	40,0	9		70	
			80						80						80	
			90						90						90	
			100						100						100	
			110						110						110	
			120						120						120	
			150						150						150	
A۱	erage Yield (I/s): 2,17	180		Ave	erage Yield	d (I/s):	4,10	180		Α	verage Yield	(l/s):	8,01	180	
	Drawdown (%): 13,12	210			Drawdow	/n (%):	23,64	210			Drawdowr	າ (%):	40,53	210	
DIS	CHARGE RA	TE 4	RPM		DIS	CHARG	E RA	TE 5	RPM]	DISCHARG	E RAT	Œ 6	RPM	
DATE	& TIME	20	20/09/28 1	6:11	DATE 8	& TIME		202	0/09/28 16:	11	DA	TE & TIME			2020/09/2	8 16:11
ГІМЕ	DRAWDOWN	YIELD	TIME	RECOVERY	TIME	DRAWD	OWN	YIELD	TIME	RECOVER	RY TIME	DRAWD	OWN	YIELD	TIME	RECOVERY
min)	(m)	(I/s)	(min)	(m)	(min)	(m)	(I/s)	(min)	(m)	(min)	(m)	1	(I/s)	(min)	(m)
	44,38		1		1				1		1				1	46,37
?	45,27		2		2				2		2				2	38,40
}	47,24	11,92			3				3		3				3	34,08
<u>, </u>	47,99	10.05	5		5				5		5				5	31,55
7	48,61	12,05	7		7				7		7				7	29,50
LO L5	49, 16 50, 33		10 15		10 15				10 15		10 15				10 15	26,76 24,57
20	51,02	12,04	_		20				20		20				20	22,07
20 30	52,07	12,01	30		30				30		30				30	19,34
10	53,27	12,03	_		40				40		40				40	16,85
50	54,08	,	50		50				50		50				50	15,43
50	55,21		60		60				60		60				60	14,10
			70						70						70	12,70
			80						80						80	11,84
			90						90						90	11,03
			100						100						100	10,37
		1	110						110						110	9,73
			120						120						120	9,18
		1	150						150						150	7,93
		-	180	-					180						180	6,90
		+	210	-					210				+		210	6,23
A -	erage Yield (I/s	. 42.02	240	-	Α	erage Yield	d (Ue).	0,00	240		-	Vorage Vield	(1/0):	0.00	240	5,64
AV	verage Yield (I/s Drawdown (%	<u> </u>	300 360		AVE	Drawdow	` ,	0,00	300 360		A	verage Yield Drawdowr		0,00	300 360	4,78 3,02
ATLIM I	EVEL ABOVE G			<u> </u>	1	awaow	nı (70)î			D PUMPED ?	NO	DI AWQOWI	1 (/0):		JUUU	3,02
	NATER LEVEL A				mbdl1:	14,66				WATER CLE						
		5, 21				,										
						STEPP	ED DI	RAWDO	WN SUM	MARY						
STEP	DURATION	DRAWDO		AVERAGE		OVERY		STEP	DURATION	DRAWD		AVERAGE			RECOVER	
	[min]	[m]	[%]		min]	[m]	[%]		[min]	[m]	[%]	YIELD [I/s]	[min]	\perp	[m]	[%]
1		4,11	13,12	2,17				5		0,00		0,00				
2		5,42	23,64	4,10				6		0,00		0,00		+		
		3,59 5,21	40,53 51,34	8,01 12,03				7 8								
3	60 5	J,Z 1						TOTAL:	240,00	55,21	51,34		0	+	0,00	0,00
4			2020/na/-	/X 1 / · · · ·				· · · · · ·	_ ~~U,UU		U 1.U+		ı	- 1		0,00
4 ATE &	TIME END:		2020/09/2	28 17:11						,	- ,-				0,00	
4 ATE &	TIME END:		2020/09/2	28 17:11												
4	TIME END:		2020/09/2		ABLISHI	MENT				13,21		ESTAE	BLISHM	ENT D		2020/09/28
4 PATE & COMME	TIME END:	BOREH				MENT MOVE		BOREH			LAGE		BLISHM ANCE E		ATE:	2020/09/28



	HOLE NO:			OLE	CON	STANT DISC	EVEL [mbdl]: HARGE 113		14,66 RECOVERY			R LEVEL [mbgl]:	14,08
	DISCHARGE	BORE	HOLE	2	_	SERVATION			SERVATION	HOLE 2	OF	SERVATION	HOLE 3
DISCHARGE BOREHOLE TEST STARTED				1	ER LEVEL [mbcl]:	N/A	WATER LEVEL [mbcl]:		N/A	WATER LEVEL [mbcl]:		N/A	
DATE & TIME: 2020/09/30 11:10				-1	SING HEIGHT [m]:	N/A	CASING HEIGHT [m]: CASING DIAMETER [m]:		N/A	-1	SING HEIGHT [m]:	N/A	
TEST COMPLETED			-	G DIAMETER [m]:	N/A	CASING DIAMETER [m]:				N/A			
D/	ATE & TIME:	2	020/10/0	02 11:10	1	DISTANCE [m]:	N/A		DISTANCE [m]:	N/A		DISTANCE [m]:	N/A
ГІМЕ	DRAWDOWN	YIELD	TIME	RECOVERY	TIME:	DRAWDOWN	RECOVERY	TIME:	DRAWDOWN	RECOVERY	TIME:	DRAWDOWN	RECOVER
[min]	[m]	[l/s]	[min]	[m]	[min]	[m]	[m]	[min]	[m]	[m]	[min]	[m]	[m]
1	7,40		1	53,43	1			1			1		
2	11,75		2	51,63	2			2			2		
3	14,90	7,65	3	49,93	3			3			3		
5	19,32	0.07	5	47,70	5			5			5		
7	22,89	8,27	7 10	45,46 42,85	7 10			7 10			7 10		
15	25,32 29,44		15	39,39	15			15			15		
20	33,07		20	36,50	20			20			20		
30	36,50	8,26	30	32,30	30			30			30		
40	39,74	0,20	40	28,85	40			40			40		
60	43,37		60	24,64	60			60			60		
90	47,68	8,25	90	19,80	90			90			90		
120	50,70		120	16,40	120			120			120		
150	52,58		150	13,79	150			150			150		
180	54,11		180	11,70	180			180			180		
210	55,30		210	10,01	210			210	· ·		210		
240	56,27	8,24	240	8,59	240			240			240		
300	57,87		300	6,24	300			300			300		
360	59,10		360	4,49	360			360			360		
420	65,43		420	2,94	420			420			420		
480	66,85		480	1,82	480			480			480		
540	67,23	8,23	540	0,85	540			540			540		
600	67,35		600	0,30	600			600			600		
720	68,41		720	0,00	720			720			720		
840	68,76	8,24	840		840			840			840		
960 1080	69,15		960 1080		960 1080			960			960 1080		
1200	69,17 69,20	8,22	1200		1200			1080 1200			1200		
1320	69,30	0,22	1320		1320			1320			1320		
1440	69,40		1440		1440			1440			1440		
	55, 15				1560			1560			1560		
					1680			1680			1680		
					1800			1800			1800		
					1920			1920			1920		
					2040			2040			2040		
					2160			2160			2160		
					2280			2280			2280		
					2400			2400			2400		
					2520			2520			2520		ļ
					2640			2640			2640		
					2760			2760			2760		
					2880			2880			2880		
					3000			3000			3000		
					3120			3120			3120		
\dashv					3240			3240			3240		
					3360 3480			3360			3360		
					3600			3480 3600			3480 3600		
					3720			3720			3720		
					3840			3840			3840		
					3960			3960			3960		
\exists					4080			4080			4080		
					4200			4200			4200		
					4320			4320			4320		
	URATION TOTA	LS [min1	CDT:	1440		RECOVERY:	1440	OBS 1:	0	OBS 2:	0	OBS 3:	0
	/DOWN / RECOV			69,40		RECOVERY:	0,00	OBS 1:	0,00	OBS 2:	0,00	OBS 3:	
DRAWDOWN / RECOVERY [%] CDT: 64,53				RECOVERY:	100,00	OBS 1:		OBS 2:	0,00	OBS 3:			
UKAW				8,23	_	COMMENTS:							



	Summary									
Applicable	Method	Sustainable yield (I/s)	Std. Dev	Early 1	Γ (m²/d)	Late T (m²/d)	S	AD used		
	Basic FC				2 0.3		2.20E-03	151.4	0).57	
	Advanced FC									
	FC inflection point									
	Cooper-Jacob	1.02	0.66			1.2	2.11E-03	151.4	1_0/132/19	
	FC Non-Linear									
	Barker	0.83	0.28	K _f =	310	S _s =	1.00E-07	151.4	0),833	
	Average Q sust (I/s)	0.91	0.35	b =	0.10	Fractal dimension n =	1.61			
		'			•				!	
	Recommended abstraction rate (L/s)		0.91		l/hr	For 24 hrs per day	4		A .	9 Schubert Road
	Hours per day of pump				l/hr	12 hrs per day				Walmer Heights
	Hours per day of pump Hours per day of pump				I/hr	10 hrs per day				Port-Elizabeth
	nours per day of pump	oing (L/s) 8	1.58	5688	I/hr	8 hrs per day				6070 South Africa
ı	Amount of water allowed to	2358.72	m ³			_			South Africa	
	Borehole could satisfy the basic human need of		3145 persons					OHS GRO	OUNDWATER	T +27 (0) 82 099 2366
	Is the water suitable for domestic use (Yes/No)		-	persons			_		TING SERVICES	E divan@dhsgroundwater.co. W https://dhsgroundwater.co
	Recommended pump depth below surface (m) Total Casing length Blow yield (l/s) Expected dynamic water level over 24hr pump Critical depth that water level must not exceeded Depth of BH Static Water Level			209 - 75 mbcl metres below casing level 155 mbcl				Divan Stroebel lydrogeologis DHS Groundwo 5/10/2021		
	Management re The aquifer consists of a good An available drawdown of 155 As a rule of thumb, 60% of the A dynamic water level of 75 mt The water level should not exce Consistent drawdown below the	sustainability.								



Scenic route 565 t/a Welltek Services Vat nr: 45902 54720 Email: welltekservices@gmail.com



Services

Cell: +27 (0)71 031 5086
Fax: +27 (0)86 517 9242

Borehole testing and associated projects

CC Registration nr: 2005/137492/23 18 Highfield Road, EAST LONDON, 5205 Cell: +27 (0)71 031 5086 Fax: +27 (0)86 517 9242

			(F) (i) (i) (i) (ii) (ii) (ii) (ii) (ii)	
		В	OREHOLE TEST RECORD	
Borehole Number:	VALLEY VIEW	BH 1	Province:	EASTERN CAPE
Alternative Number:			District:	LOERIE
Coordinates: Latitude [°S]	33,880178		Town/Village/Farm:	VALLEY VIEW
Longitude [°E]	25,001164		Rig Type & number:	NISSAN
Date & Time Test Started:	2021/04/21 00	0:00	Operator:	JUNIOR
Date & Time Test Ended:	2021/04/28 00	0:00	Supervisor:	HERMAN
Consultant:			-	
CONSULTANT - DATA PR	OVIDED / INST	RUCTIONS:		EXISTING INSTALLATION:
Borehol	e depth [mbgl]:		Diesel/Electric/Wind/Hand	N/A
 	Blow Yield [I/s]:		Pump Make & Serial no:	N/A
Water Strike D	epth(s) [mbgl]:		Intallation Depth (m)	N/A
Installation	n depth [mbgl]:		Type & Condition - Pump:	N/A
Estimated Step	s [l/s] - Step 1:		- Column:	N/A
	Step 2:		- Pump House	N/A
	Step 3:			FIELD MEASUREMENTS:
	Step 4:		Depth Before Test [mbcl]:	209,00
	Step 5:		Depth after Test [mbcl]:	209,00
	Step 6:		Water Level before Test [mbcl]:	4,25
Step	Duration [min]:		Water Level after Test [mbcl]:	6,38
Step Recovery	Duration [Hrs]:		Casing Depth [mbcl]:	PVC
Cons	tant Yield [I/s]:		Casing Height [magl]:	0,23
Constant	Duration [Hrs]:		Casing Diameter [mm]:	186,00
Recovery Duration [Hrs] /	Drawdown %:			TEST PUMP INSTALLATION DETAILS:
Lenghth of Layfla	t Required [m]:		Pump Used:	BP 30 M
Frequency of pH and EC	Measurements:		Depth Installed [mbcl]:	160,00
SAMPLE IN	STRUCTIONS:		Datum Level above Casing [m]:	0,65
			Length of Layflat [m]:	100,00
			GENERAL ACTIONS:	
Supplied new steel of	cover [Yes/No]:	NO	Slug Test [Yes/No]:	N/A
Velded existing steel cover	back on [Y/N]:	YES	Re-install existing pum	p [Yes/No]: N/A
Borehole Ma	rking [Yes/No]:	NO	If not, where was it stored?	N/A
Site Cleaning and Finis	shing [Yes/No]:	YES	Maintenance work [Hrs]:	N/A
Data Reporting and Reco	rding [Yes/No]:	YES	Maintenance Travel [km]:	N/A
Digital Photo Ta	aken? [Yes/No]	NO	List of parts replaced/repaired:	N/A
RETREAT	FROM SITE		Date &Time Sampled:	NO SAMPLE TAKEN
It is hereby acknowledged the existing equipment is in an ac			COM	IMENTS BY ONSITE CREW
NAME:]	
DESIGNATION:				
SIGNATURE:				
DATE:				



BOREHO	DLE NO: VA	LLEY VIEW	BH1 W	VATER LEVEL			4,90			TH [mbgl]:	4,02	A	VAILAB	LE DRAW	DOWN [m]:	155,75
DV	SOUL DOD D	mp 1	DDM							RECOVER	RY	DIGGILLE	GD D		DDM	
	SCHARGE RA		RPM 21/04/21 1	14.20		SCHARO	JE RA		RPM 1/04/21 12:	20		DISCHAR ATE & TIME	GE RA	ATE 3	RPM	24 42-20
TIME	DRAWDOWN	YIELD	TIME	RECOVER			/DOWN	YIELD	TIME	RECOVE			/DOWN	YIELD	2021/04/ TIME	RECOVERY
(min)	(m)	(I/s)	(min)	(m)	(min)		n)	(I/s)	(min)	(m)	(mir		m)	(l/s)	(min)	(m)
1	2,23	, ,	1	, ,	1	7,	56	, ,	1	` '	1	23	, 18	, ,	1	. ,
2	3, 10		2	<u> </u>	2		00	1,12	2		2		,27	4,84	2	
3	3,93	0,89	3		3		40	1.00	3		3		,40	0.05	3	
5 7	5,03 5,22	0,75	5 7		5 7		50 ,80	1,22	5 7		5 7		,10 ,52	3,05 2,52	5 7	
10	5,25	0,73	10		10		,57	1,22	10		10		,56	2,02	10	
15	5,28	3,.2	15		15		,53		15		15		,70	2,52	15	
20	5,37	0,7	20		20	13	,04	1,20	20		20	46	,44		20	
30	5,78	0,68	30		30		,66		30		30		,40	2,53	30	
40	6,05	0.05	40	-	40	_	,38	1.01	40		40		,27	0.50	40	
50 60	6,25 6,42	0,65	50 60	-	50 60		,88 ,24	1,21	50 60		50 60		, 13 , 21	2,53	50 60	
00	0,42		70		- 00	10	, 2/1		70		- 00	J-1	, 21		70	
			80						80						80	
			90						90						90	
			100						100						100	
			110	 					110			-			110	
			120 150	-					120 150						120 150	1
A	 verage Yield (I/s): 0,68	180	+	A	verage Yie	eld (l/s):	1,21	180			Average Yie	ld (l/s):	2,59	180	
	Drawdown (%		210	1		Drawdo			210			Drawdo		34,81	210	
DIS	SCHARGE RA	TE 4	RPM		Di	SCHAR	GE RA	TE 5	RPM			DISCHAR	GE RA	ATE 6	RPM	
DATE	& TIME	20	21/04/21 1	4:30	DATE	& TIME		202	1/04/21 14:	30	D.	ATE & TIME			2021/04/	21 14:30
TIME	DRAWDOWN	YIELD	TIME	RECOVER	Y TIME	DRAW	/DOWN	YIELD	TIME	RECOVE	RY TIM	E DRAW	/DOWN	YIELD	TIME	RECOVERY
min)	(m)	(I/s)	(min)	(m)	(min)	(r	m)	(I/s)	(min)	(m)	(mir	1) (1	m)	(l/s)	(min)	(m)
1	58,32	+	1	-	1				1		1				1	94,83
2 3	63,76 67,27	3,76	3		3				3		3				3	84, 13 76, 80
5 5	72,37	3,70	5		5				5		5				5	64,66
<u></u> 7	77,54	4,18	7		7				7		7				7	57,86
10	83,90		10		10				10		10				10	46,49
15	93,05	4,18	15		15				15		15				15	35,77
20	99,39	4.15	20		20				20		20				20	18,66
30 40	109,38 121,16	4,15	30 40		30 40				30 40		30 40				30 40	15,33 13,96
10 50	136,99	4,07	50		50				50		50				50	12,47
60	148,82	1 3,51	60		60				60		60				60	11,42
			70						70						70	10,48
			80	<u> </u>					80						80	10,00
			90	 					90			-			90	9,38
			100	+					100			-+			100	8,99 8 53
			110 120	+					110 120			-			110 120	8,53 8,24
			150	†					150						150	7,23
			180						180						180	7,09
			210						210						210	6,85
		,	240	 	-				240						240	6,53
A	verage Yield (I/s Drawdown (%		300 360	1	A	verage Yie Drawdo			300 360			Average Yie		0,00	300 360	6,21
DATUM	Drawdown (%			3		PLSM00	wii (%):	<u> </u>		D PUMPED	? NO	Drawdo	wii (%):	l	Joou	6,07
	WATER LEVEL A				[mbdl]:	4,90				WATER CL		}				
		DD4	NAM	T.,,,,,,			PED D	RAWDO	WN SUM		DOM:				DECC:	
STEP	DURATION	DRAWD([m]	OWN [%]	AVERAGE YIELD [I/s]	[min]	COVERY [m]	[%]	STEP	DURATION [min]	DRAW [m]	DOWN [%]	AVERAGE YIELD [I/s]		in1	RECOVER [m]	RY [%]
1		6,42	4,12	0,68	·1	E2	1.41	5	<u> </u>	0,00	1,01	0,00	1	-	P-9	1,~1
2	60	5,24	9,78	1,21				6		0,00		0,00				
3		54,21	34,81	2,59				7								
4		48,82	95,55	4,11				8	0/0	4/2	0= ==				0.00	
OATE &	TIME END:		2021/04/2	21 15:30				TOTAL:	240,00	148,82	95,55		0)	0,00	0,00
OIVIIVIE	.1113.															
				ES	TABLISH	MENT						ESTA	ABLISH	IMENT D	ATE:	2021/04/21
		PODELI	OL F				-	DODEL					TANIO -	DETME	EN.	
	MOVEROM:	BOREH	ULE	VILL	AGE	MOV	╘╟	BOREH	OLE	VIL	LLAGE	DIS	IANCE	BETWE	EN	392,00



	UUKE	HOLE NO:	VA	LLEIV	IEW BH 1	COM		EVEL [mbdl]: HARGE TE		4,90 RECOVERY		vv/AIEK	R LEVEL [mbgl]:	4,02
Test Standard St		DISCHARGE	BORE	HOLE	3						HOLE 2	OF	SERVATION	HOLE 3
						_			1			1		N/A
	D.				22 07:00	4			-1			-1		N/A
March Marc		TEST	COMPLE	TED		4			CASIN	G DIAMETER [m]:		CASIN	G DIAMETER [m]:	N/A
Min	D.	ATE & TIME:	2	021/04/2	27 07:00	1	DISTANCE [m]:	N/A		DISTANCE [m]:	N/A	1	DISTANCE [m]:	N/A
1	ГІМЕ	DRAWDOWN	YIELD	TIME	RECOVERY	TIME:	DRAWDOWN	RECOVERY	TIME:	DRAWDOWN	RECOVERY	TIME:	DRAWDOWN	RECOVERY
2 S. S. S. 2 2 197.39 2 3 102.00 3 3 3 3 3 3 3 3 3	[min]		[l/s]	1		1	[m]	[m]	1 -	[m]	[m]	1	[m]	[m]
3						1			1			t -		
5 9.97 1.48 5 5 97.89 5 5 7 7 11.23 2.56 7 91.85 7 7 11.23 2.56 7 91.85 7 7 11.23 2.56 7 91.85 7 7 11.23 2.56 7 91.85 7 7 10 13.17 10 87.56 10 10 10 10 10 10 10 10 10 10 10 10 10			4.00	1		1								
7 1123 2,56 7 91,85 7 91,85 7 91,85 10 10 10 13,17 10 10 13,17 10 15 15,26 10 15 15 15 15 15 15 15					1									
10 13.17						1								
15		•	2,56	1		1								
20		•	2.55			+ -								
30		•		i		1			1					
40 33,47 2,53 40 60,30 40 40 40 40 40 40 40			2,00	t		1			1			1		
60	40		2.53			+			1			1		
99 63.03 2,52 90 51,96 90 90 90 90 90 90 90 90 90 90 90 90 90	60		1,,,,,			-			<u> </u>					
120	90	,	2,52											
150	120			1		1			1					
180	150					1								
240	180		2,52	180		180			180			180		
1000	210	68,73		210	43,87	210			210			210		
1860	240	70,25		240	43,05	240			240			240		
120	300	71,35	2,51	300	42,22	300			300			300		
180	360	71,86		360	40,65	360			360			360		
S40	420	72,26		420	39,30	420			420			420		
Second S	480	72,78	2,50	480	38,22	480			480			480		
	540	74,21		540	36,64	540			540			540		
May State State	600		2,53	1		1								
	720					1								
1080 92,53 1080 29,46 1080	840	•				1								
200	960	•	2,55	1		1								
320	1080	•		1		1			1					
Hard			0.50	i		1			1					
10,20		•		t		1			1			1		
112,44			2,31	1		1						1		
113,75			2 53	1		+			1			1		
920	1800		2,00			1								
115,10	1920		2.52			1								
160	2040		_,-,			1						1		
280	2160		2,50	1								1		
Auton 118,36	2280	•	Ľ											
120,42	2400		2,51	2400	18,67	2400						2400		
Tell	2520	119,54		2520	17,34	2520			2520			2520		
120	2640	120,42		2640	16,47	2640			2640			2640		
120	2760	121,59	2,50	2760	15,89	2760			_			2760		
120	2880	122,39		2880	15,03	1			1			1		
240	3000		2,51	ļ		1								
3360 12,16 3360 3360 3360 3360 3480 3480 3480 3480 3480 3480 3480 3480 3480 3480 3480 3480 3480 3480 3480 3600 3600 3600 3600 3600 3600 3720 3840	3120													
A80	3240		2,50			_								
600 128,72 3600 3600 3600 720 129,28 2,53 3720 3720 3720 840 130,36 3840 3840 3840 3840 960 131,56 2,52 3960 3960 3960 080 132,72 4080 4080 4080 4080 200 133,64 2,50 4200 4200 4200 4200 320 134,91 4320 4320 4320 4320 4320 DURATION TOTALS [min] CDT: 4320 RECOVERY: 2880 OBS 1: 0 OBS 2: 0 OBS 3: 0 IRAWDOWN / RECOVERY [%] CDT: 134,91 RECOVERY: 15,03 OBS 1: 0,00 OBS 2: 0,00 OBS 3: 0, AVERAGE YIELD [I/s] CDT: 2,51 COMMENTS: COMMENTS: COMMENTS: 0 OBS 2: 0,00 OBS 3: 0,00	3360													
129,28	3480		2,50						1					
840	3600		2.52	-		1			1					
960 131,56 2,52 3960 3960 3960 4080 4080 4080 200 133,64 2,50 4200 4200 4200 4200 320 134,91 4320 4320 4320 4320 4320 4320 200 200 200 200 200 200 200 200 200			2,53											
080 132,72			2 52			1						1		
200 133,64 2,50 4200 4200 4200 4200 4320 4320 4320 4320 4320 4320 4320 4320 4320			2,32	<u> </u>		1			1			1		
320 134,91 4320 4320 4320 4320	4200		2 50	1		-			1			1		
DURATION TOTALS [min] CDT: 4320 RECOVERY: 2880 OBS 1: 0 OBS 2: 0 OBS 3: 0 JRAWDOWN / RECOVERY [m] CDT: 134,91 RECOVERY: 15,03 OBS 1: 0,00 OBS 2: 0,00 OBS 3: 0, RAWDOWN / RECOVERY [%] CDT: 86,62 RECOVERY: 88,86 OBS 1: 0,00 OBS 2: 0,00 OBS 3: 0, AVERAGE YIELD [I/s] CDT: 2,51 COMMENTS: COMMENTS: OMB 2: 0,00 OBS 3: 0,	4320	-	2,30			+			1			1		
RAWDOWN / RECOVERY [m] CDT: 134,91 RECOVERY: 15,03 OBS 1: 0,00 OBS 2: 0,00 OBS 3: 0,			J S [min1	CDT.	4320	•	RECOVERY:	2880		0	OBS 2:		OBS 3:	0
RAWDOWN / RECOVERY [%] CDT: 86,62 RECOVERY: 88,86 OBS 1: 0,00 OBS 2: 0,00 OBS 3: 0,														
AVERAGE YIELD [I/s] CDT: 2,51 COMMENTS:									1					
								,	,	-,		-,		-,
GENERAL ITEMS AND MAINTENANCE TRAVELING FOR VERIFICATION [km]: TRANSPORT EXISTING EQUIPMENT [km]: TRANSPORT EXISTING EQUIPMENT [km]:										IANCE	_ 			



15.5 Appendix 5: Laboratory Reports

Final Report

Pathcare, St George's Hosp 40 Park Drive Central P.E. Tel: 041 391 5700



Report to:

Referred by: WISTERIA PAKHUIS (PTY) LTD

WISTERIA PAKHUIS (PTY) LTD ATT: BELINDA SMITH

ATT: BELINDA SM PO BOX 254 6335 PATENSIE

Requisition No: 810386768 Patient: (RefNo: BELINDA SMITH) Guarantor:

pecimen No: 0815:BS00057R
collection Date: 2022-08-15 08:00

WISTERIG 2-MAGALIES FARM WATER
Patient ID No: N/A

WISTERIA PAKHUIS (PTY) LTD
Contact No: 0793377923

 Specimen No:
 0815:BS00057R
 WISTERIG 2-MAGA

 Collection Date:
 2022-08-15 08:00
 Patient ID No:
 N/A

 Received Date:
 2022-08-15 12:00
 Age:Sex:DoB:
 U

 Reported Date:
 2022-08-29 16:18
 Contact No:
 N/A

Tests requested: SANS 241 DRINKING WATER

	Biochemis	try		
Test Name	Result	Flag	Reference Range	
RISK: Operational				
ALUMINIUM	< 15		0-300 ug/L	
PH VALUE	7.4		5.0-9.7 pH units	
TURBIDITY	3		NTU	
Guidelines: Operational Aesthetic		0-1 0-5	NTU NTU	
RISK: Aesthetic				
AMMONIA N	< 0.1		0-1.5 mg/L	
CHLORIDE	218		0-300 mg/L	
CONDUCTIVITY mS/m @ 25 C	105.00		0-170 mS/m	
SODIUM	145		0-200 mg/L	
TOTAL DISSOLVED SOLIDS	681		0-1200 mg/L	
TURBIDITY	3		NTU	
Guidelines: Operational Aesthetic		0-1 0-5	NTU NTU	
ZINC	< 0.20		0-5 mg/L	
WATER COLOUR	34	Н	0-15 mg/l Pt	
ISK: Acute Health 1				
CYANIDE FREE/TOTAL	< 10		0-200 ug/L	
NITRATES	< 0.18		0-11 mg/L	
NITRITE	0.0		0-0.9 mg/L	
RISK: Chronic health				
ANTIMONY	< 7		0-20 ug/L	
ARSENIC (As)	< 7		0-10 ug/L	
CADMIUM (Cd)	< 1		0-3 ug/L	
CHROMIUM (Cr)	< 4		0-50 ug/L	
COPPER (Cu)	< 50		0-2000 ug/L	
FLUORIDE	0.2		0-1.5 mg/L	
LEAD (Pb)	< 6		0-10 ug/L	
MERCURY (Hg)	< 4		0-6 ug/L	
NICKEL	< 5		0-70 ug/L	
SELENIUM	< 15		0-40 ug/L	

Generated: 2022-08-29 16:18 Page 1 of 2



(H20)

BORON (WATER ANALYSIS)

Report to: WISTERIA PAKHUI	S (PTY) LTD	Requisition No: 810386768	Patient: WISTERIG 2-MAGALIES FARM WATER
RISK: Multiple			
IRON		310	ug/L
	Guidelines: Aesthetic Chronic health	0-300 0-2000	
MANGANESE		150	ug/L
	Guidelines: Aesthetic Chronic health	0-100 0-400	ug/L ug/L
SULPHATES		48	mg/L
	Guidelines: Aesthetic Acute health	0-250 0-500	
Reference:			
	Samples from th different resul Water testing w subsidiary, Bem Accreditation n For a list of a 021 8531490 or	e specific only to the samp e same or similar source ma t. as performed by Pathcare's lab Pty Ltd	ay deliver a wholly owned contact Bemlab at
BARIUM (Ba) (H2	0)	131	0-700 ug/L
FREE CHLORINE	, ,	0.02	0-5 mg/L
	Guidelines: Chronic health	< 5 mc	g/L
URANIUM (U) (H2	20)	< 12	0-30 ug/L
TOTAL ORGANIC	CARBON	< 5	0-10 mg/L

Authorised on 2022-08-29 15:48:00
For consultation, contact a Pathologist - 0413915700
H=High, L=Low, *H=Critically High, *L=Critically Low, #=Delta Checked
In rare cases, analytical interference may cause erroneous results.
Please inform pathologist if results and clinical picture do not concur.
~ File [] Phone Patient [] Appointment [] Prescription [] Draw File []

240

0-2400 ug/L



Pathcare, St George's Hosp 40 Park Drive Central P.E. Tel: 041 391 5700



Guarantor:

Report to: Referred by: WISTERIA PAKHUIS (PTY) LTD

WISTERIA PAKHUIS (PTY) LTD ATT: BELINDA SMITH PO BOX 254 6335 PATENSIE

Requisition No: 810386769 Patient: (RefNo: BELINDA SMITH) Specimen No: 0815:BS00051R

WISTERIA PAKHUIS (PTY) LTD Contact No: 0793377923 WISTERIA 2-MAGALIES FARM WATER

Collection Date: 15-08-2022 UNK Patient ID No: N/A 2022-08-15 12:00 Age:Sex:DoB: Received Date: U Reported Date: 2022-08-29 16:18 Contact No: N/A

Clinical Data:

WISTERIA 2-MAGALIES FARM BH2
Please note that the collection date or time was not
provided and could not be verified by PathCare.

Tests requested: SANS 241 DRINKING WATER

		Biochemis	try		
Test Name		Result	Flag	Reference Range	
RISK: Operational					
ALUMINIUM		< 15		0-300 ug/L	
PH VALUE		7.3		5.0-9.7 pH units	
TURBIDITY		14		NTU	
	elines: ational netic		0-1 0-5	NTU NTU	
RISK: Aesthetic					
AMMONIA N		0.1		0-1.5 mg/L	
CHLORIDE		181		0-300 mg/L	
CONDUCTIVITY mS/m @	25 C	84.60		0-170 mS/m	
SODIUM		114		0-200 mg/L	
TOTAL DISSOLVED SOL	IDS	550		0-1200 mg/L	
TURBIDITY		14		NTU	
	elines: ational netic		0-1 0-5	NTU NTU	
ZINC		< 0.20		0-5 mg/L	
WATER COLOUR		127	Н	0-15 mg/l Pt	
RISK: Acute Health 1					
CYANIDE FREE/TOTAL		< 10		0-200 ug/L	
NITRATES		0.22		0-11 mg/L	
NITRITE		0.0		0-0.9 mg/L	
RISK: Chronic health					
ANTIMONY		< 7		0-20 ug/L	
ARSENIC (As)		< 7		0-10 ug/L	
CADMIUM (Cd)		< 1		0-3 ug/L	
CHROMIUM (Cr)		< 4		0-50 ug/L	
COPPER (Cu)		< 50		0-2000 ug/L	
FLUORIDE		0.3		0-1.5 mg/L	
LEAD (Pb)		< 6		0-10 ug/L	
MERCURY (Hg)		< 4		0-6 ug/L	

Generated: 2022-08-29 16:18 Page 1 of 2



	to: WISTERIA PAKHU		isition No: 810386769	Patient: WISTERIA 2-MAGALIES FARM	
	NICKEL		< 5	0-70 ug/L	
	SELENIUM		< 15	0-40 ug/L	
RISK: I	Multiple				
	IRON		990	ug/L	
		Guidelines: Aesthetic Chronic health	0- 0-	-300 ug/L -2000 ug/L	
	MANGANESE		80	ug/L	
		Guidelines: Aesthetic Chronic health	0- 0-	-100 ug/L -400 ug/L	
	SULPHATES		23	mg/L	
		Guidelines: Aesthetic Acute health	0- 0-	-250 mg/L -500 mg/L	
efere	nce:			g , -	
			*		
	BARIUM (Ba) (H:	021 8531490 or email Guidelines as per SA	ecific only to the le or similar source of similar source of the left of left of the left of left of the left of t	ce may deliver a re's wholly owned ease contact Bemlab at	
		0-0-1-0-1-0-1-0-1-0-1-0-1-0-1-0-1-0-1-0	0.03	0-5 mg/L	
	FREE CHLORIN	Guidelines: Chronic health		5 mg/L	
			< 12	0-30 ug/L	
	URANIUM (U) (H				
	URANIUM (U) (H TOTAL ORGANI (H20)		< 5	0-10 mg/L	

Authorised on 2022-08-29 15:52:00
For consultation, contact a Pathologist - 0413915700
H=High, L=Low, *H=Critically High, *L=Critically Low, #=Delta Checked
In rare cases, analytical interference may cause erroneous results.
Please inform pathologist if results and clinical picture do not concur.
~ File [] Phone Patient [] Appointment [] Prescription [] Draw File []



Pathcare, St George's Hosp 40 Park Drive Central P.E. Tel: 041 391 5700



Report to:

Referred by: WISTERIA PAKHUIS (PTY) LTD

WISTERIA PAKHUIS (PTY) LTD ATT: BELINDA SMITH PO BOX 254 6335 PATENSIE

Requisition No: 810386766
 Specimen No:
 0815:BS00054R

 Collection Date:
 2022-08-15 08:15

Received Date: 2022-08-15 12:45 Reported Date: 2022-08-29 15:58

Patient: (FileNo: NOT SUPPLIED) (RefNo: BELINDA SMITH)

U WISTERIA 2 - SPOORBRUG B WATER
Patient ID No: 22:810386766

Age:Sex:DoB: U Contact No: 0410001515 Guarantor:

WISTERIA PAKHUIS (PTY) LTD Med Aid: CLIENTS Member No: NOT AVAILABLE Contact No: 0793377923

Tests requested: SANS 241 DRINKING WATER

ICD10 code(s): Z76.9				
	Biochemis	try		
Test Name	Result	Flag	Reference Range	
RISK: Operational				
ALUMINIUM	< 15		0-300 ug/L	
PH VALUE	7.1		5.0-9.7 pH units	
TURBIDITY	12		NTU	
Guidelines: Operational Aesthetic		0-1 0-5	NTU NTU	
RISK: Aesthetic				
AMMONIA N	< 0.1		0-1.5 mg/L	
CHLORIDE	226		0-300 mg/L	
CONDUCTIVITY mS/m @ 25 C	93.60		0-170 mS/m	
SODIUM	128		0-200 mg/L	
TOTAL DISSOLVED SOLIDS	608		0-1200 mg/L	
TURBIDITY	12		NTU	
Guidelines: Operational Aesthetic		0-1 0-5		
ZINC	< 0.20		0-5 mg/L	
WATER COLOUR	102	Н	0-15 mg/l Pt	
RISK: Acute Health 1				
CYANIDE FREE/TOTAL	< 10		0-200 ug/L	
NITRATES	< 0.18		0-11 mg/L	
NITRITE	0.0		0-0.9 mg/L	
RISK: Chronic health				
ANTIMONY	< 7		0-20 ug/L	
ARSENIC (As)	< 7		0-10 ug/L	
CADMIUM (Cd)	< 1		0-3 ug/L	
CHROMIUM (Cr)	< 4		0-50 ug/L	
COPPER (Cu)	< 50		0-2000 ug/L	
FLUORIDE	0.3		0-1.5 mg/L	
LEAD (Pb)	< 6		0-10 ug/L	
MERCURY (Hg)	< 4		0-6 ug/L	
NICKEL	< 5		0-70 ug/L	

Generated: 2022-08-29 15:58

Page 1 of 2



	AKHUIS (PTY) LTD Requ	isition No: 810386766		Patient: U WISTERIA 2 - SPOORBRUG B WATER
SELENIUM		< 15		0-40 ug/L
RISK: Multiple				
IRON		690		ug/L
	Guidelines: Aesthetic Chronic health		0-300 0-2000	
MANGANES		410		ug/L
	Guidelines: Aesthetic Chronic health		0-100 0-400	ug/L ug/L
SULPHATES		31		mg/L
	Guidelines: Aesthetic Acute health		0-250 0-500	
Reference:				
	Sampling done by cli			
	Test results are spe Samples from the sam different result.	cific only to t	he samp urce ma	ole tested. ay deliver a
	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number	cific only to t e or similar so rformed by Path ty Ltd T0654	urce ma	wholly owned
	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P	cific only to te or similar so rformed by Path ty Ltd T0654 ited analytes, admin@bemlab.c	care's please	wholly owned contact Bemlab at
BARIUM (Ba	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA	cific only to te or similar so rformed by Path ty Ltd T0654 ited analytes, admin@bemlab.c	care's please	wholly owned contact Bemlab at
	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA a) (H20) DRINE (WATER)	cific only to te or similar so rformed by Path ty Ltd T0654 ited analytes, admin@bemlab.cNS 241-1:2015 D	care's please	wholly owned contact Bemlab at g water.
	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA a) (H20) DRINE (WATER) Guidelines:	cific only to te or similar so rformed by Path ty Ltd T0654 ited analytes, admin@bemlab.cNS 241-1:2015 D 94	urce ma care's please o.z rinking	wholly owned contact Bemlab at g water. 0-700 ug/L 0-5 mg/L
·	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA (H2O) DRINE (WATER) Guidelines: Chronic health	cific only to te or similar so rformed by Path ty Ltd T0654 ited analytes, admin@bemlab.cNS 241-1:2015 D 94	care's please	wholly owned contact Bemlab at g water. 0-700 ug/L 0-5 mg/L
FREE CHLC	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA (H2O) DRINE (WATER) Guidelines: Chronic health	cific only to te or similar so rformed by Path ty Ltd T0654 ited analytes, admin@bemlab.c NS 241-1:2015 D 94 0.05	urce ma care's please o.z rinking	wholly owned contact Bemlab at g water. 0-700 ug/L 0-5 mg/L

Authorised on 2022-08-29 15:39:00
For consultation, contact a Pathologist - 0413915700
H=High, L=Low, *H=Critically High, *L=Critically Low, #=Delta Checked
In rare cases, analytical interference may cause erroneous results.
Please inform pathologist if results and clinical picture do not concur.
~ File [] Phone Patient [] Appointment [] Prescription [] Draw File []



Pathcare, St George's Hosp 40 Park Drive Central P.E. Tel: 041 391 5700



Report to:

Referred by: WISTERIA PAKHUIS (PTY) LTD

WISTERIA PAKHUIS (PTY) LTD ATT: BELINDA SMITH PO BOX 254 6335 PATENSIE

Requisition No: 810386767

Specimen No: 0815:BS00055R Collection Date: 2022-08-15 08:00 Received Date: 2022-08-15 12:45 Reported Date: 2022-08-29 15:59 **Patient:** (FileNo: NOT SUPPLIED) (RefNo: BELINDA SMITH)

WISTERIA 2-SPOORBRUG BH2 WATER
Patient ID No: 22:810386767

Age:Sex:DoB: Contact No: 0410001515

Guarantor: WISTERIA PAKHUIS (PTY) LTD

Med Aid: CLIENTS Member No: NOT AVAILABLE U Contact No: 0793377923

Tests requested: SANS 241 DRINKING WATER

ICD10 code(s): 776.9

	Biochemis	try		
Test Name	Result	Flag	Reference Range	
RISK: Operational				
ALUMINIUM	< 15		0-300 ug/L	
PH VALUE	6.9		5.0-9.7 pH units	
TURBIDITY	46		NTU	
Guidelines: Operational Aesthetic		0-1 0-5		
RISK: Aesthetic				
AMMONIA N	< 0.1		0-1.5 mg/L	
CHLORIDE	191		0-300 mg/L	
CONDUCTIVITY mS/m @ 25 C	80.00		0-170 mS/m	
SODIUM	106		0-200 mg/L	
TOTAL DISSOLVED SOLIDS	520		0-1200 mg/L	
TURBIDITY	46		NTU	
Guidelines: Operational Aesthetic		0- <u>1</u> 0-5	NTU NTU	
ZINC	< 0.20		0-5 mg/L	
WATER COLOUR	202	Н	0-15 mg/l Pt	
RISK: Acute Health 1				
CYANIDE FREE/TOTAL	< 10		0-200 ug/L	
NITRATES	< 0.18		0-11 mg/L	
NITRITE	0.0		0-0.9 mg/L	
RISK: Chronic health				
ANTIMONY	< 7		0-20 ug/L	
ARSENIC (As)	< 7		0-10 ug/L	
CADMIUM (Cd)	< 1		0-3 ug/L	
CHROMIUM (Cr)	< 4		0-50 ug/L	
COPPER (Cu)	< 50		0-2000 ug/L	
FLUORIDE	0.3		0-1.5 mg/L	
LEAD (Pb)	< 6		0-10 ug/L	
MERCURY (Hg)	< 4		0-6 ug/L	
NICKEL	< 5		0-70 ug/L	

Generated: 2022-08-29 15:59

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SELENIUM		< 15		0-40 ug/L
RISK: Multiple				
IRON		4100		ug/L
	Guidelines: Aesthetic Chronic health		0-300 0-2000	
MANGANES	SE	580		ug/L
	Guidelines: Aesthetic Chronic health		0-100 0-400	
SULPHATE	· — · · · · · · · · · · · · · · · · · ·	31		mg/L
	Guidelines: Aesthetic Acute health		0-250 0-500	
Reference:				
Reference:	Sampling done by cli Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA	cific only to the or similar sour rformed by Pathot ty Ltd T0654 ited analytes, padmin@bemlab.cons 241-1:2015 Dr	are's lease	wholly owned contact Bemlab at
BARIUM (B.	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA a) (H20)	cific only to the or similar sour rformed by Pathot ty Ltd T0654 ited analytes, padmin@bemlab.cons 241-1:2015 Dr	are's lease	wholly owned contact Bemlab at water. 0-700 ug/L
BARIUM (B.	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA a) (H20) ORINE (WATER)	cific only to the or similar sour rformed by Pathot ty Ltd T0654 ited analytes, padmin@bemlab.cons 241-1:2015 Dr	are's lease	wholly owned contact Bemlab at
BARIUM (B.	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA a) (H20)	cific only to the or similar sourformed by Pathoty Ltd T0654 ited analytes, padmin@bemlab.co	are's lease	wholly owned contact Bemlab at water. 0-700 ug/L 0-5 mg/L
BARIUM (B.	Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA a) (H20) ORINE (WATER) Guidelines: Chronic health	cific only to the or similar sourformed by Pathoty Ltd T0654 ited analytes, padmin@bemlab.co	are's lease .za inking	wholly owned contact Bemlab at water. 0-700 ug/L 0-5 mg/L
BARIUM (B. FREE CHLO URANIUM (Test results are spe Samples from the sam different result. Water testing was pe subsidiary, Bemlab P Accreditation number For a list of accred 021 8531490 or email Guidelines as per SA a) (H20) ORINE (WATER) Guidelines: Chronic health	cific only to the or similar sourformed by Pathoty Ltd T0654 ited analytes, padmin@bemlab.co	are's lease .za inking	wholly owned contact Bemlab at water. 0-700 ug/L 0-5 mg/L

Authorised on 2022-08-29 15:43:00
For consultation, contact a Pathologist - 0413915700
H=High, L=Low, *H=Critically High, *L=Critically Low, #=Delta Checked
In rare cases, analytical interference may cause erroneous results.
Please inform pathologist if results and clinical picture do not concur.
~ File [] Phone Patient [] Appointment [] Prescription [] Draw File []



Pathcare, St George's Hosp 40 Park Drive Central P.E. Tel: 041 391 5700



Report to: Referred by: WISTERIA PAKHUIS (PTY) LTD

WISTERIA PAKHUIS (PTY) LTD ATT: BELINDA SMITH PO BOX 254 6335 PATENSIE

Requisition No: 810386770 Patient: (RefNo: BELINDA SMITH)

 Patient: (RefNo: BELINDA SMITH)
 Guarantor:

 U WISTERIA2-VALLEY VIEW BH WATER
 WISTERIA PAKHUIS (PTY) LTD

 Patient ID No:
 N/A
 Contact No:
 0793377923

 Specimen No:
 0815:BS00056R
 U WISTERIA2-VALL

 Collection Date:
 2022-08-15 08:30
 Patient ID No:
 N/A

 Received Date:
 2022-08-15 12:00
 Age:Sex:DoB:
 U

 Reported Date:
 2022-08-29 16:18
 Contact No:
 N/A

Clinical Data: WISTERIA2-VALLEY VIEW BH3
Tests requested: SANS 241 DRINKING WATER

		Biochemis	try		
Test Name		Result	Flag	Reference Range	
RISK: Operational					
ALUMINIUM		17		0-300 ug/L	
PH VALUE		8.2		5.0-9.7 pH units	
TURBIDITY		9		NTU	
	Guidelines: Operational Aesthetic		0-1 0-5		
RISK: Aesthetic					
AMMONIA N		< 0.1		0-1.5 mg/L	
CHLORIDE		225		0-300 mg/L	
CONDUCTIVITY m	S/m @ 25 C	99.00		0-170 mS/m	
SODIUM		136		0-200 mg/L	
TOTAL DISSOLVE	D SOLIDS	644		0-1200 mg/L	
TURBIDITY		9		NTU	
	Guidelines: Operational Aesthetic		0-1 0-5	NTU NTU	
ZINC		< 0.20		0-5 mg/L	
WATER COLOUR		75	Н	0-15 mg/l Pt	
RISK: Acute Health 1					
CYANIDE FREE/TO	OTAL	< 10		0-200 ug/L	
NITRATES		< 0.18		0-11 mg/L	
NITRITE		0.0		0-0.9 mg/L	
RISK: Chronic health					
ANTIMONY		< 7		0-20 ug/L	
ARSENIC (As)		< 7		0-10 ug/L	
CADMIUM (Cd)		< 1		0-3 ug/L	
CHROMIUM (Cr)		< 4		0-50 ug/L	
COPPER (Cu)		< 50		0-2000 ug/L	
FLUORIDE		0.7		0-1.5 mg/L	
LEAD (Pb)		< 6		0-10 ug/L	
MERCURY (Hg)		< 4		0-6 ug/L	
NICKEL		< 5		0-70 ug/L	
SELENIUM		< 15		0-40 ug/L	

Generated: 2022-08-29 16:18 Page 1 of 2



Report to: WIS	STERIA PAKHUIS	(PTY) LTD	Requisition No: 8103867	70	Patient: U WISTERIA2-VALLEY VIEW BH WATER
RISK: Multip	le				
IRO	ON		410		ug/L
		Guidelines: Aesthetic Chronic health		0-300 0-2000	ug/L D ug/L
MA	NGANESE		< 50		ug/L
		Guidelines: Aesthetic Chronic health		0-100 0-400	ug/L
SU	LPHATES		25		mg/L
		Guidelines: Aesthetic Acute health		0-250 0-500	
Reference:					
		Samples from th different resul Water testing w subsidiary, Bem Accreditation n For a list of a 021 8531490 or	e specific only to e same or similar : t. as performed by Pa lab Pty Ltd	chcare's please	ay deliver a wholly owned contact Bemlab at
ВА	RIUM (Ba) (H20		112		0-700 ug/L
	EE CHLORINE		0.14		0-5 mg/L
		Guidelines: Chronic health		< 5 mg	7/1
UR	ANIUM (U) (H20		< 12	, J III,	0-30 ug/L
	TAL ORGANIC		< 5		0-10 mg/L
ВО	RON (WATER A	ANALYSIS)	140		0-2400 ug/L

Authorised on 2022-08-29 15:56:00
For consultation, contact a Pathologist - 0413915700
H=High, L=Low, *H=Critically High, *L=Critically Low, #=Delta Checked
In rare cases, analytical interference may cause erroneous results.
Please inform pathologist if results and clinical picture do not concur.
~ File [] Phone Patient [] Appointment [] Prescription [] Draw File []







A Level 1 B-BBEE company

[006431/22], [2022/08/10]

Certificate of Analysis

Project details

Customer Details

Company name:	DHS GROUNDWATER CONSULTING SERVICES	
Contact address:	9 SCHUBERT ROAD, PORT ELIZABETH, 6070	
Contact person:	DIVAN STROEBEL	

Sampling Details

Sampled by:	CUSTOMER
Sampled date:	2022/07/26

Sample Details

Sample type(s):	GROUNDWATER SAMPLES
Date received:	2022/08/01
Delivered by:	CUSTOMER - PORT ELIZABETH LAB
Temperature at sample receipt (°C):	2.7
Deviations:	020384/22,020385/22,020386/22,020387/22 - Inappropriate bottle type submitted for bacteriological testing

Report Details

Testing commenced:	2022/08/01	
Testing completed:	2022/08/10	
Report date:	2022/08/10	
Our reference:	006431/22	



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Talbot Laboratories (Pty) Ltd

Analytical Results

Methods	Determinands	Units	020384/22	020385/22
			JFBH1 26.07.2022	ALBH1 26.07.2022
Chemical				
85	Dissolved Calcium	mg Ca/l	12.9	NR
85	Potassium	mg K/ℓ	7.28	NR
85	Dissolved Magnesium	mg Mg/l	21	NR
84	Sodium	mg Na/ℓ	136	NR
83A	Copper	μg Cu/ℓ	1.3	NR
83A	Iron	μg Fe/l	70	NR
83A	Manganese	μg Mn/ℓ	1415	NR
83A	Lead	μg Pb/ℓ	<1	NR
10G	Total Alkalinity	mg CaCO₃/ℓ	16.1	NR
16G	Chloride	mg Cl/ℓ	255	NR
123	Free Chlorine*	mg Cl₂/ℓ	0.10	<0.1
122	Monochloramine*	mg/l	<3	<3
40A	Colour (True)*	mg Pt-Co/l	<10	<10
2A	Electrical Conductivity at 25°C	mS/m	108	82.9
18G	Fluoride	mg F/Ł	0.42	NR
65Gc	Nitrate	mg N/l	<0.25	NR
65Gb	Nitrite	mg N/l	<0.05	NR
Calc.	Combined Nitrate + Nitrite (sum of Ratios)*	-	<0.12	NR
4	Turbidity	NTU	17	23
1	pH at 25°C	pH units	5.9	6.3
67G	Sulphate	mg SO ₄ /ℓ	40.1	NR
Calc.	Total Hardness*	mg CaCO₃/ℓ	120	NR
Microbiolo	ogical			
32	E. coli*	MPN/100ml	<1^	<1^
32	Total Coliforms*	MPN/100ml	517^	14^
31	Standard Plate Count*	colonies/ml	>1000^	43^



Reference: [006431/22] Page 2 of 5



Talbot Laboratories (Pty) Ltd

Methods	Determinands	Units	020386/22	020387/22
			JMBH1 27.07.2022	BJBH1 27.07.2022
Chemical				
85	Dissolved Calcium	mg Ca/ℓ	8.52	NR
85	Potassium	mg K/ℓ	18.4	NR
85	Dissolved Magnesium	mg Mg/l	16.3	NR
84	Sodium	mg Na/l	59	NR
83A	Copper	μg Cu/ℓ	234	NR
83A	Iron	μg Fe/l	388	NR
83A	Manganese	μg Mn/ℓ	59	NR
83A	Lead	µg Pb/ℓ	7.4	NR
10G	Total Alkalinity	mg CaCO₃/ℓ	90	NR
16G	Chloride	mg Cl/ℓ	100	NR
123	Free Chlorine*	mg Cl₂/ℓ	<0.1	<0.1
122	Monochloramine*	mg/l	<3	<3
40A	Colour (True)*	mg Pt-Co/l	<10	<10
2A	Electrical Conductivity at 25°C	mS/m	61.4	80.9
18G	Fluoride	mg F/l	0.24	NR
65Gc	Nitrate	mg N/l	<0.25	NR
65Gb	Nitrite	mg N/l	<0.05	NR
Calc.	Combined Nitrate + Nitrite (sum of Ratios)*	=	<0.12	NR
4	Turbidity	NTU	4.0	9.4
1	pH at 25°C	pH units	6.6	7.6
67G	Sulphate	mg SO₄/ℓ	11.5	NR
Calc.	Total Hardness*	mg CaCO₃/ℓ	88	NR
Microbiolo	gical			
32	E.coli*	MPN/100ml	<1^	<1^
32	Total Coliforms*	MPN/100ml	<1^	70^
31	Standard Plate Count*	colonies/ml	22^	76^

Refer to the "Notes" section at the end of this report for further explanations.

Where the laboratory reporting limit for a test is higher than the required specification limit, the raw data is reviewed and the detection limit highlighted in bold font if outside of specification.

Where a deviation has been noted, the validity of the results may be affected. Results should be used with this consideration in mind.

Specific Observations

Results that appear in bold do not meet the specification limits in Appendix 1 of this report.



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Talbot Laboratories (Pty) Ltd

Quality Assurance

Technical signatories

Notes to this report

Limitations

This report shall not be reproduced except in full without prior written approval of the laboratory. Results in this report relate only to the samples as taken, and the condition received by the laboratory. Any opinions and interpretations expressed herein are outside the scope of SANAS accreditation.

The decision rule applicable to this laboratory is available on request.

Sample preparation may require filtration, dilution, digestion or similar. Final results are reported accordingly. Where the laboratory has undertaken the sampling, the location of sampling and sampling plan are available on request. Talbot Laboratories is guided by the National Standards SANS 5667-3:2006 Part 3 Guidance on the

Preservation and Handling of Water Samples; SANS 5667-1:2008 Part 1 Guidance on the Design of Sampling Programmes and Sampling Techniques and SANS 5667-2:1991 Part 2: Guidance on Sampling Techniques. Customers to contact Talbot Laboratories for further information.

Uncertainty of measurement

Talbot Laboratories' Uncertainty of Measurement (UoM) values are:

- Identified for relevant tests.
- Calculated as a percentage of the respective results.
- Applicable to total, dissolved and acid soluble metals for ICP element analyses.
- Available upon request.

Analysis explanatory notes

Tests may be marked as follows:

٨	Tests conducted at our Port Elizabeth satellite laboratory.
*	Tests not included in our Schedule of Accreditation and therefore that are not SANAS accredited.
#	Tests that have been sub-contracted to a peer laboratory.
NR	Not required -shown, for example, where the schedule of analysis varied between samples.
σ	Field sampling point on-site results.
a	Testing has deviated from Method.



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